# Hybrid Control of a 3-D Structure by using Seismic isolators and Semi-Active Dampers

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### Goal

During strong seismic ground motions

- Base isolators shall not rupture
- Structural response should not be badly affected

Seismic Isolator displacement

Structural displacement

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- Intro: Control of Seismic isolated Structures
- 3-story building model
- semi active hydraulic damper
- Control Design
  - Linear Quadratic Regulator(LQR)
  - Upper Controller
- Response simulation
- **⇒** Results



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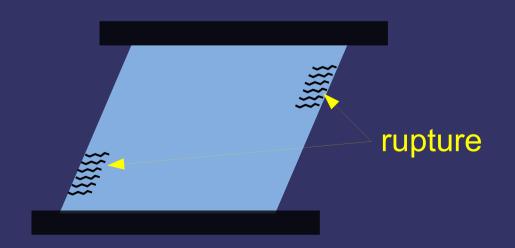
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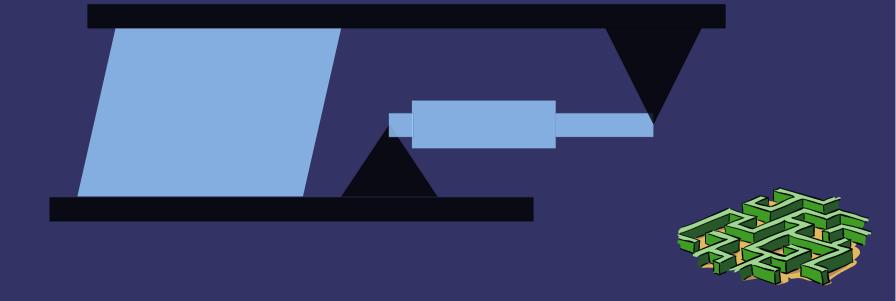


- Base Isolator: Rupture at large displacements
- → Damper: Increases the impedance (dynamic rigidity) of the structure
- Solution: Adjustable damping foce

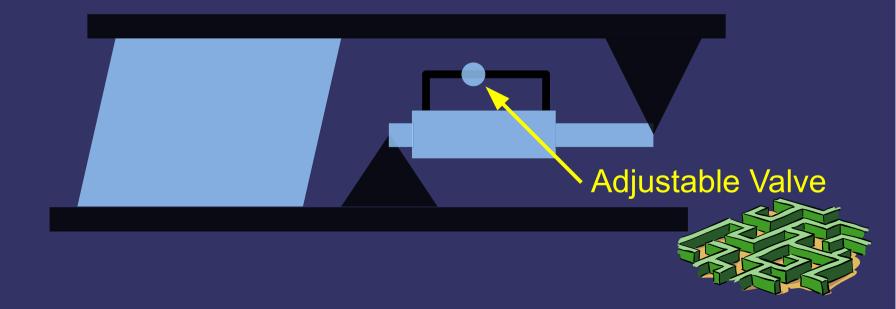




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- → Wongprasert & Symans (2005) → Building model with variable orifice damping - using fuzzy logic
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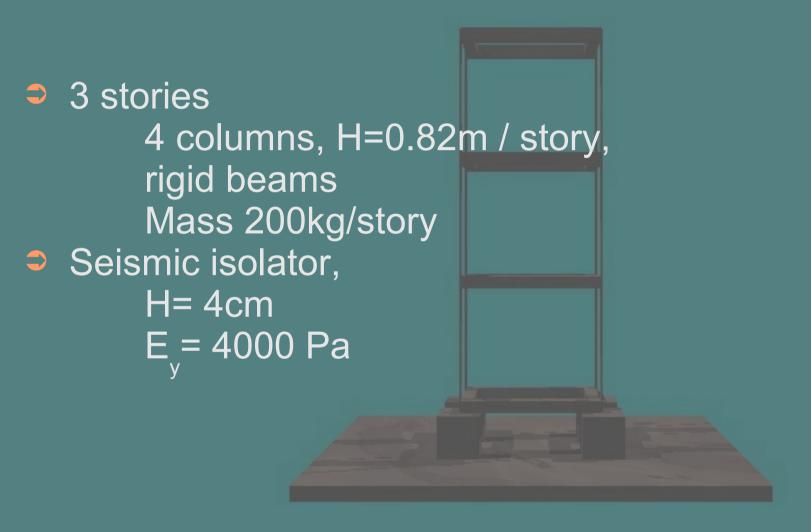
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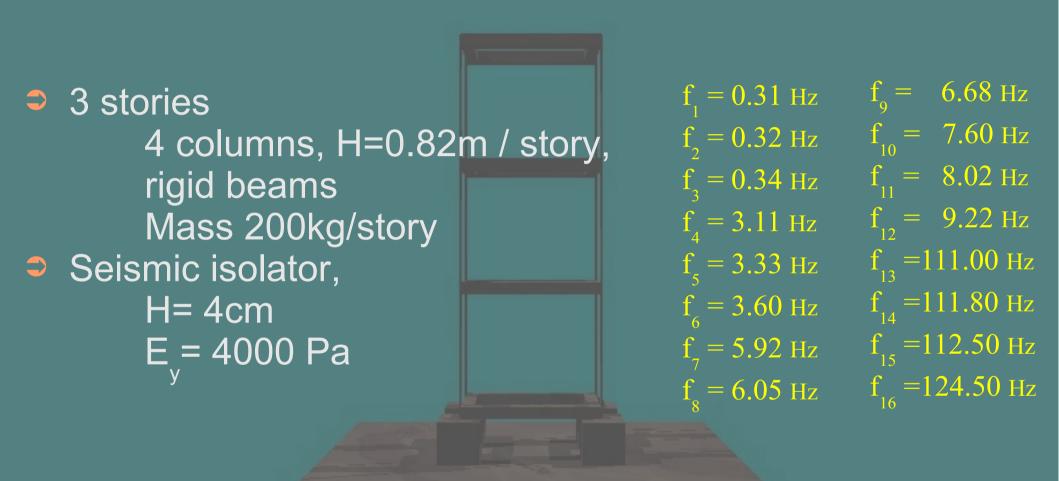
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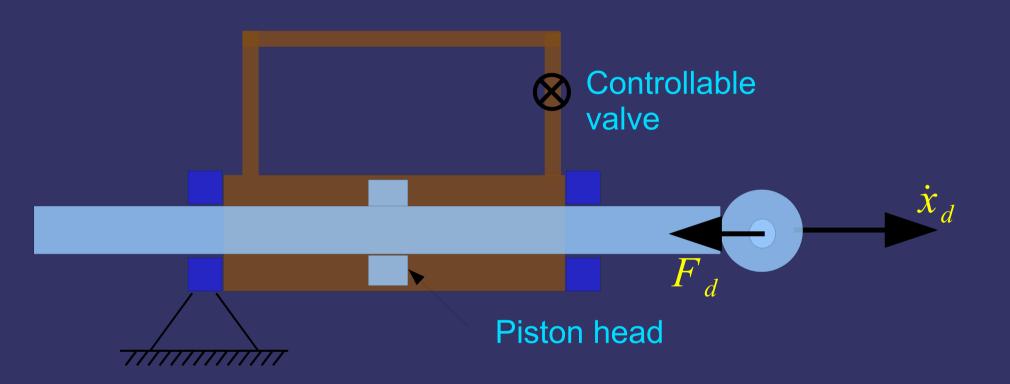
### **Building Model**



# **Building Model**



# Damper with adjustable valve (semi active damper)



$$F_d \approx -c_d \dot{x}_d$$

$$5000 \frac{N \cdot s}{m} < c_d < 25000 \frac{N \cdot s}{m}$$



$$\mathbf{M} \ddot{x} + (\mathbf{C} + \mathbf{\Gamma}_d \mathbf{C}_d \mathbf{\Gamma}_d^T) \dot{x} + \mathbf{K} x = -\mathbf{M} \mathbf{\Gamma}_{eq} \ddot{x}_{eq}$$



$$\begin{split} \mathbf{M} \, \ddot{x} + (\mathbf{C} + \boldsymbol{\Gamma}_d \, \boldsymbol{C}_d \, \boldsymbol{\Gamma}_d^T) \, \dot{x} + \mathbf{K} \, x &= -\mathbf{M} \, \boldsymbol{\Gamma}_{eq} \, \ddot{x}_{eq} \\ \mathbf{M} \, \ddot{x} + (\mathbf{C} + \boldsymbol{\Gamma}_d \, \boldsymbol{C}_d \, \boldsymbol{\Gamma}_d^T) \, \dot{x} + \mathbf{K} \, x &= -\mathbf{M} \, \boldsymbol{\Gamma}_{eq} \, \ddot{x}_{eq} + \boldsymbol{\Gamma}_d \, u \end{split}$$



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2nd order diff. Equation --> 1st order diff.Eqn.

$$\dot{q} = A q + B_1 \ddot{x}_g + B_2 u$$



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2nd order diff. Equation --> 1st order diff.Eqn.

$$\dot{q} = A q + B_1 \ddot{x}_g + B_2 u$$

Here, 
$$q = \begin{bmatrix} x & \dot{x} \end{bmatrix}^T$$

$$A = \begin{bmatrix} 0 & I \\ -\mathbf{M}^{-1}\mathbf{K} & -\mathbf{M}^{-1}(\mathbf{C} + \mathbf{\Gamma}_d \mathbf{C}_d \mathbf{\Gamma}_d^T) \end{bmatrix} \qquad B_1 = \begin{bmatrix} 0 \\ \mathbf{\Gamma}_{eq} \end{bmatrix} \quad B_2 = \begin{bmatrix} 0 \\ \mathbf{M}^{-1} \mathbf{\Gamma}_d \end{bmatrix}$$

$$B_1 = \begin{bmatrix} 0 \\ \Gamma_{eq} \end{bmatrix} \quad B_2 = \begin{bmatrix} 0 \\ \Gamma_{eq} \end{bmatrix}$$



# Control Design: (LQR)

Minimization problem

$$V(q) = \int_{0}^{\infty} q^{T} Q q + u^{T} R u dt$$

Kontrol force contribution

Structural response contribution

# Control Design: (LQR)

The optimal control force that minimizes the problem definition

$$u^o = -R^{-1}B_2^T \bar{P} q^o$$

Here,  $\bar{P}$  is the solution to the following Ricatti equation

$$A^{T}\bar{P} + \bar{P}A + Q - \bar{P}B_{2}R^{-1}B_{2}^{T}\bar{P} = 0$$



- Damping levels: 5000 : 5000 : 25000 Ns/m
  5 positions / damper
- No. of dampers = 4

#### Therefore

- 625 damping configurations, and thus
- 625 optimal control equations
   (The minimization problem is solved for 625 different configurations)

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- No. of dampers = 4

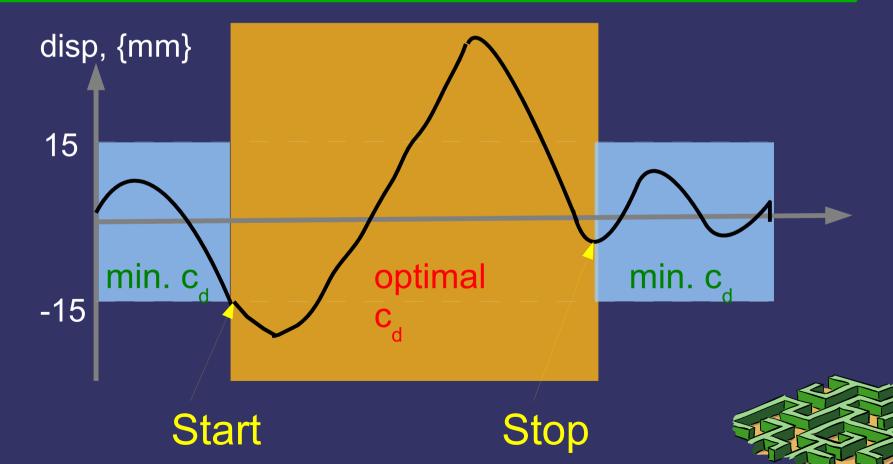
#### **Therefore**

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- d<sub>base</sub> < 15mm → minimum damping
- ⇒ d<sub>base</sub> > 15mm → optimal damping



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- ⇒ d<sub>base</sub> > 15mm → optimal damping



At time t<sub>i</sub>, the upper controller

- calculates the optimal control force, u
- calculates the closest damping force to achieve the desired optimal control force
- switches to the calculated damping state



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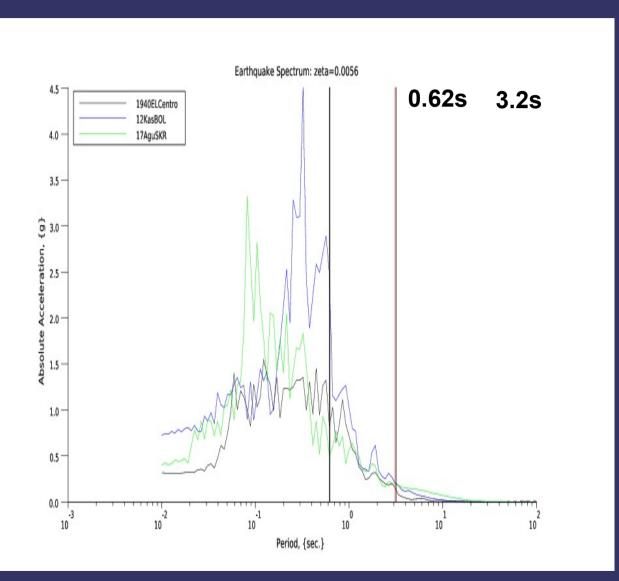
### Response simulation

### Selected Earthquakes

19.05.1940 Imperial Valley (El Centro) 12.11.1999 Düzce (Bolu) 17.08.1999 Kocaeli (Sakarya)

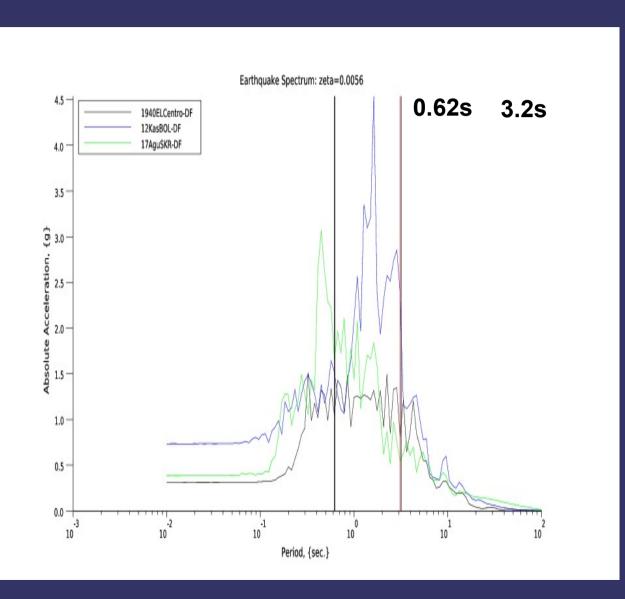
Earthquake		Date	A <sub>max</sub> ,	V <sub>max</sub> ,	D <sub>max</sub> ,
			{ <b>g</b> }	{m/s}	{m}
1	I-ELC-180	1940	0.296	0.236	0.130
	I-ELC-270	1940	0.179	0.279	0.221
2	Bolu-000	1999	0.728	0.405	0.230
	Bolu-090	1999	0.822	0.620	0.132
3	SKR-090	1999	0.317	0.284	0.442
4	I-ELC-180-DF	-	0.304	1.18	3.25
	I-ELC-270-DF	1	0.182	1.39	5.51
5	Bolu-000-DF	-	0.733	2.03	5.74
	Bolu-090-DF	-	0.830	3.10	3.30
6	SKR-090-DF	-	0.337	1.42	11.0

# Response simulation



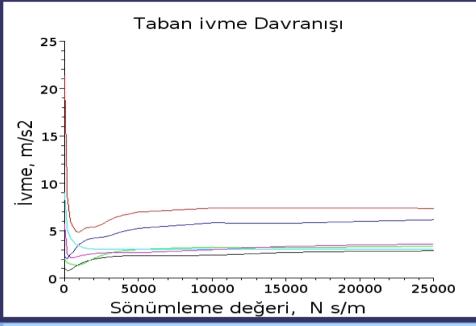
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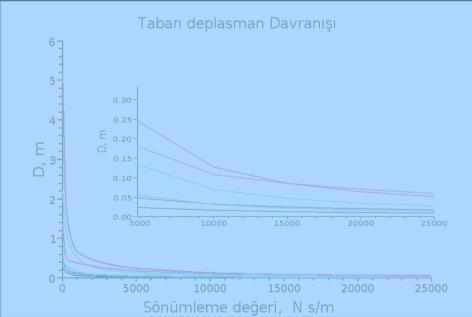


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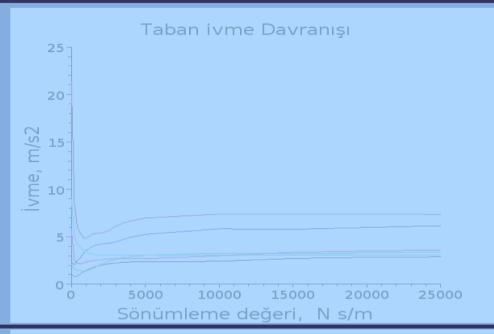


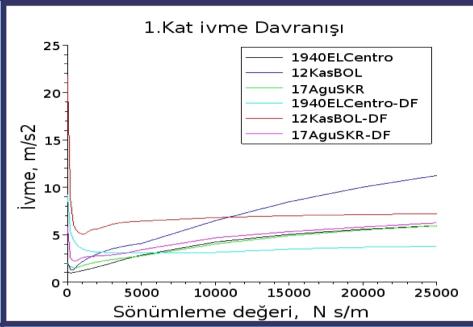


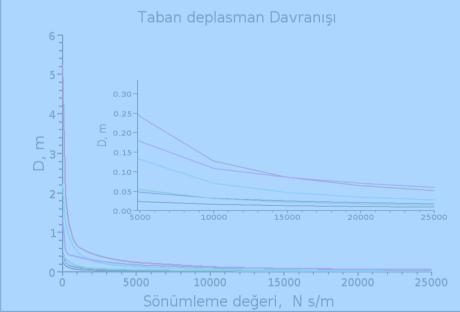




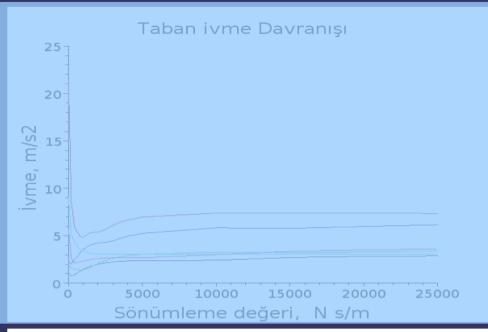




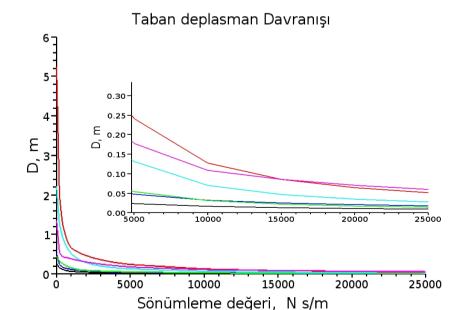


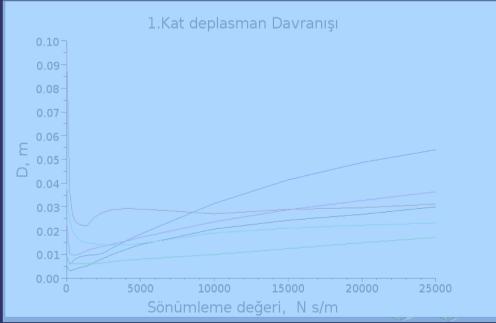


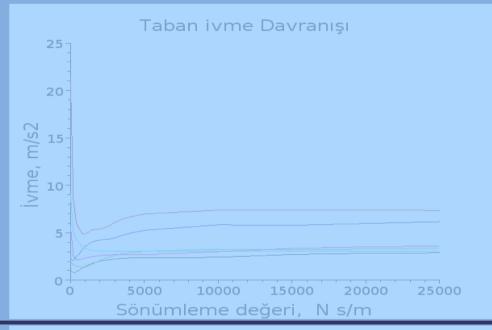


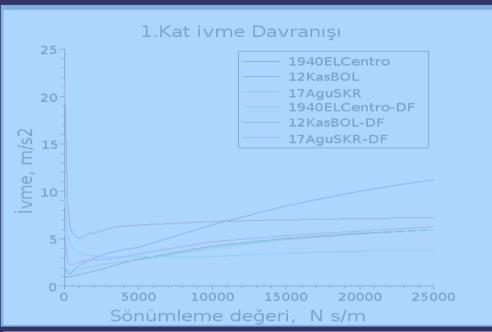


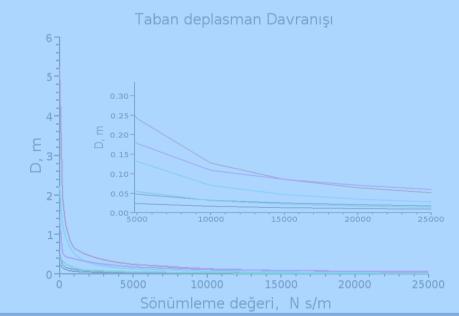


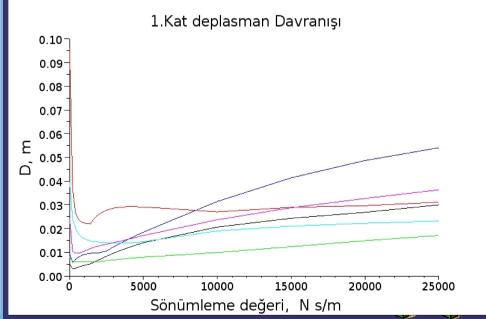


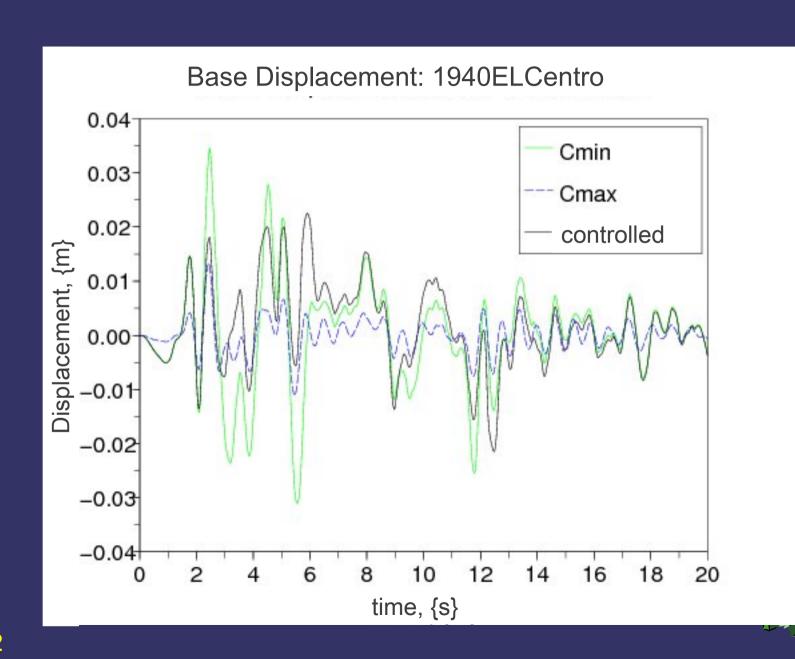


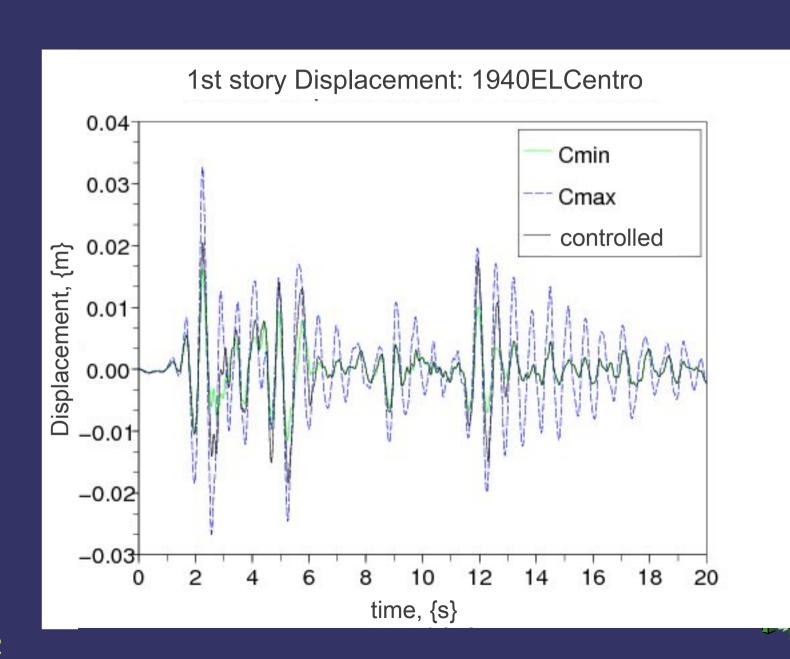


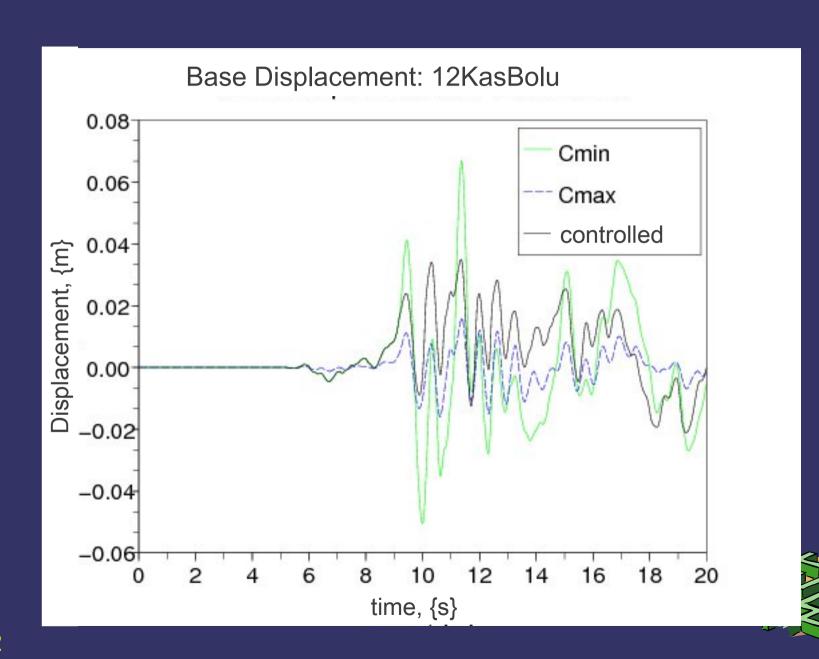


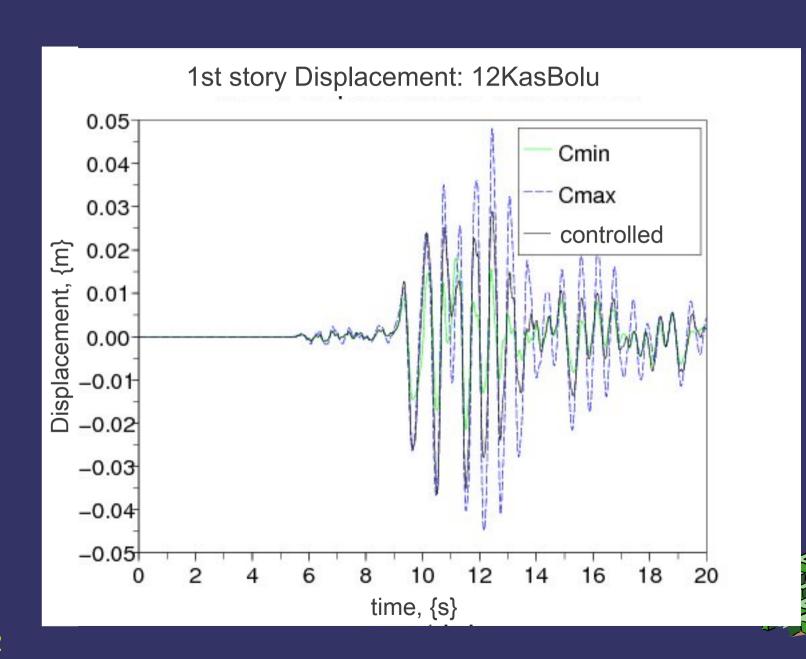


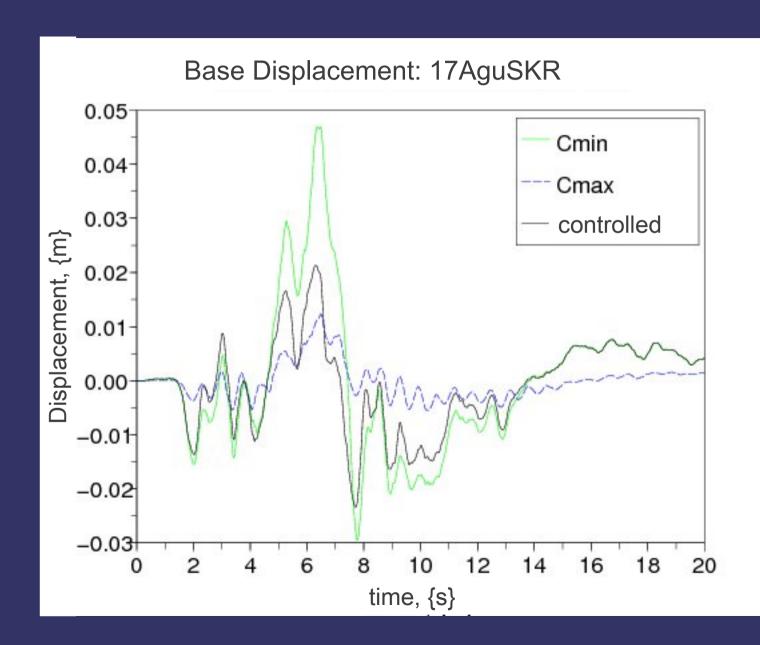


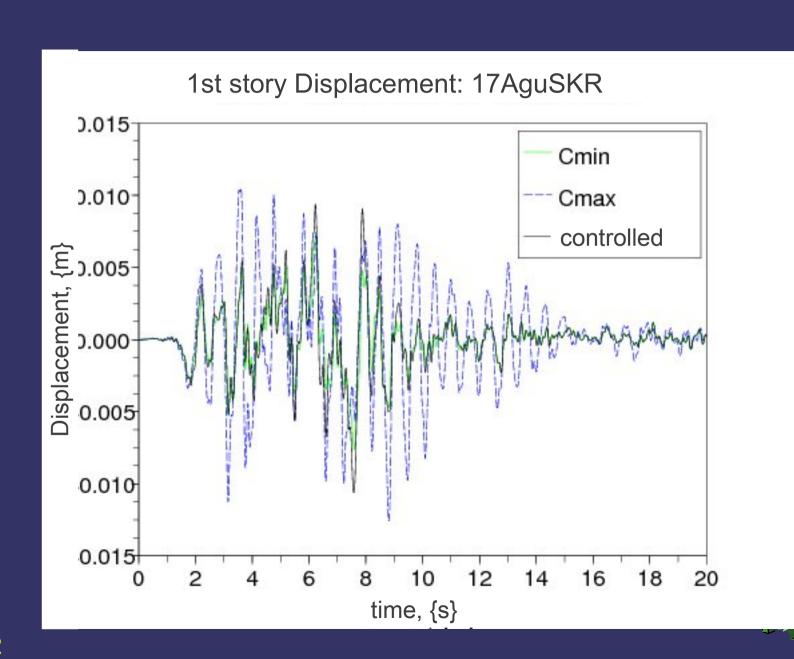












	d	C <sub>min</sub>	C <sub>max</sub>	C <sub>contr</sub>	$\frac{C_{contr} - C_{min}}{C_{min}}$
El Centro	Base {m}	0.035	0.013	0.022	-35 %
	1st story {m}	0.016	0.033	0.020	26 %
Bolu	Base {m}	0.067	0.016	0.035	-48 %
	1st story {m}	0.022	0.048	0.036	69 %
Sakarya	Base {m}	0.047	0.012	0.023	-50 %
	1st story {m}	0.0076	0.0126	0.0106	39 %



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	1st story {m}	0.022	0.048	0.036	69 %	-24 %
Sakarya	Base {m}	0.047	0.012	0.023	-50 %	90 %
	1st story {m}	0.0076	0.0126	0.0106	39 %	-16 %



#### Results

Benefits of using base isolators together with semi active dampers

- Isolator displacement is reduced (%35-%50 reduction w.r.t. min. damping case).
- ⇒ No significant increase in 1st story displacement response (%16-%37 w.r.t. max. damping)
- This control system is robust because energy is only introduced to change the valve positions of the dampers

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- No significant increase in 1st story displacement response (%16-%37 w.r.t. max. damping)
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# Thank you

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