

Problem # 1:

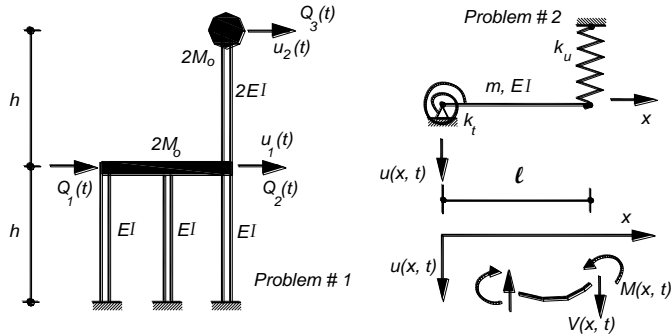
Consider the system of two degrees-of-freedom shown where the first story is rigid plate having a mass of $2M_o$ and the second story consists of a cantilever column. a. Evaluate the flexibility \mathbf{d} matrix, the mass matrix \mathbf{m} and the rigidity matrix $\mathbf{k} = \mathbf{d}^{-1}$ and the load vector \mathbf{p} . b. Determine the circular frequencies and the periods of the free vibration ω_i and T_i in terms of EI , m and h . c. Obtain the corresponding two mode shapes ϕ_i and give their graphical representation ($i=1,2$). d. Check the orthogonality of the modes with respect to the mass matrix and the stiffness matrix $\phi_1^T \mathbf{m} \phi_2$, and $\phi_1^T \mathbf{k} \phi_2$. e. Evaluate the generalized masses and stiffness

$$M_i = \phi_i^T \mathbf{m} \phi_i$$

and $K_i = \phi_i^T \mathbf{k} \phi_i$ and assess the relationship $\omega_i^2 = K_i / M_i$ ($i=1,2$).

Problem # 2:

Consider the distributed parameter system shown where m is the mass per unit length and EI is the bending rigidity of the cross section. The left end of the beam is fixed and has a rotational spring k_t . The right end of the beam is free and has a lateral spring k_u . Write down the boundary conditions for the free vibration of the beam. Obtain the frequency determinant in terms of $\beta^4 = m\ell^4 \omega^2 / (EI)$ $\beta = m\ell^4 \omega^2 / (EI)$ by assuming $M_o = m\ell$, $k_u = EI / \ell^3$ and $k_t = EI / \ell$.



$$\mathbf{m} \ddot{\mathbf{u}}(t) + \mathbf{k} \mathbf{u}(t) = \mathbf{p}(t) \quad \mathbf{u}(t) = [u_1(t) \quad u_2(t)]^T \quad \mathbf{p}(t)^T = [P_1(t) \quad P_2(t)] \quad \omega_i = 2\pi / T_i$$

$$(\mathbf{k} - \omega_i^2 \mathbf{m}) \phi_i = 0 \quad (\mathbf{I} - \omega_i^2 \mathbf{d} \mathbf{m}) \phi_i = 0 \quad |\mathbf{k} - \omega_i^2 \mathbf{m}| = 0 \quad |\mathbf{I} - \omega_i^2 \mathbf{d} \mathbf{m}| = 0 \quad M_i = \phi_i^T \mathbf{m} \phi_i$$

$$K_i = \phi_i^T \mathbf{k} \phi_i \quad M_i \ddot{Y}_i(t) + K_i Y_i(t) = \phi_i^T \mathbf{p}(t) \quad Y_i(t) = \sum_{i=1}^2 \phi_i^T \mathbf{m} \mathbf{v} / M_i \quad k = \frac{3EI}{h^3} \quad k = \frac{12EI}{h^3}$$

$$Y_i(t) = \frac{\sin \omega_i t}{M_i \omega_i} \left[\phi_i^T \int_0^{t_0} \mathbf{p}(\tau) d\tau \right] \quad L_i = \phi_i^T \mathbf{m} \mathbf{1} \quad \Gamma_i = L_i / M_i \quad M_i^* = \Gamma_i L_i$$

$$\mathbf{1}^T = [1 \quad 1] \quad u(x,t) = \sum \phi_i(x) Y_i(t) \quad \ddot{Y}_i(t) + \omega_i^2 Y_i(t) = 0 \quad M(x,t) = -EI \frac{\partial^2 u}{\partial x^2}$$

$$\phi(x) = A_1 \sin ax + A_2 \cos ax + A_3 \sinh ax + A_4 \cosh ax \quad a^4 = \frac{m \omega^2}{EI} \quad V(x,t) = -EI \frac{\partial^3 u}{\partial x^3}$$

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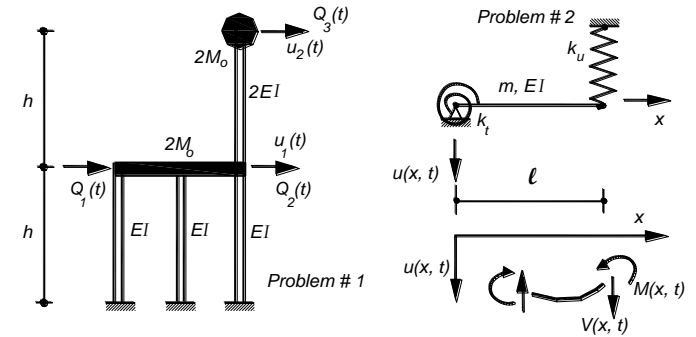
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