Determination of Loads Acting on Guide Rail Fixing Under Certain Loading Condition

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ABSTRACT

In terms of provide safety and smooth travel, guide rails and their fixing components are essential elements of the complete elevator system. Loads acting on the guide rails and fasteners occur during the elevator car normal travel lead to bending and buckling (or tensile) stresses. In this study, numerical calculations are explained according to EN 81-1 for certain loading conditions. Stress and deformations occur on the fixing components (bolts and T-clips) are examined by experimentally. Finally, the results obtained from numerical calculation and test results are compared and discussed.

1. INTRODUCTION

Elevator systems are composed of many elements. Rail brackets and steel clips are used for fixing guide rails to shaft wall and provide the linearity of the guide rails. These are the essential elements of a complete rail fastening system. Guide rails are, for safety reasons, the most important element of elevator systems. The basic functions of the guide rails and rail fasteners in the elevator system are to guide the elevator car and counterweight in their vertical travel, to minimize the horizontal movement of the car as much as possible, to prevent tilting of the car due to eccentric load, and also to provide safe stance and to stop the car during safety gear operation activated in case of free falling of the passenger car. Various forces occur during the elevator car travel, safety gear operation, and seismic activities upon on guide rails and rail fasteners. When guide rails are not mounted properly, especially during the operation of the safety brake guide rail brackets would be subjected to excessive loads. These forces on them lead to bending and buckling (or tensile) stresses effecting on fasteners and mounting elements. Review of literature about the topic shows that studies related with stress and deflection analysis of guide rails, brackets and steel T-clips generally remained limited to the computer environment (Atay 2013).

2. GUIDE RAILS, BRACKETS AND FASTENERS

In this study, fasteners under certain loading conditions were concerned. Guide rails and complete rail fastening system are shown in Figure 1.



Figure 1. Assembly of complete guide rail fixing system

Idea of examining the behaviour of elevator brackets and its connections under static and dynamic loads with an experimental study emerged from knowledge that obtained as a result of experimental stress analysis of elevator guide rails and finite element modelling and simulation studies in the Elevator (Lift) Technologies Laboratory, ITU Faculty of Mechanical Engineering, and an experimental set that is submitted by Dr. Merz from HILTI firm in the comprehensive articles (Merz 2008, 2010).



Figure 2. Brackets and T-Bolts

Bracket connection system will make displacements or relative movements under the loads applied during tests. Loads on rail brackets and its joints that for fixing guide rails to wall of the elevator shaft, studied experimentally. In this case the brackets are mounted with pre-stressed bolts (Figure 3). Wherein by the application of transverse forces between the parts, a μF_{pre} friction force, (F_{fric}) occurs. The theoretical principles of fasteners are given for making the mechanical joint effective (1).

$$F_{fric} = \mu F_{pre} \ge F/i$$
 or $\mu F_{pre} = c_0 F/i$ (1)

Where i is the number of bolts and $c_0 = 1.1 - 1.5$ is the safety factor against sliding. From this equation, the force necessary to provide the joint can be found.



Figure 3. Bolts under transverse loads

M12 bolts and T3 T-bolts are suitable for T90 guide rails in accordance to the standards (Imrak and Gerdemeli, 2000).

3. TEST SETUP

Those parts that make up the basic elements of the elevator system, examination of the behaviour of the different load cases, monitoring and new constructive measures to be taken to investigate an experimental set was designed and installed for the purpose. Experiments to be made by using this experimental set; with the basic elements of the elevator system is aimed to obtain tangible concrete data. For an experimental study on the guide rail brackets and its connections, possibilities within the experimental set system was designed and established with the support and contributions of the sponsor companies. The experimental set, designed, which was tried to have the qualities that will allow for compliance reports and research and investigation to be made more comprehensive in the future on a variety of guide rail brackets and its connections. This experimental set system consists of four main structures. These are carrier structural frame that is used to connect the elements to be tested in experimental studies, hydraulic power unit that provides variable loads to be applied, control-drive unit and sensors. The carrier structural frame is used to connect the experimental elements, which is made of St37 material, is a structure formed by the method of welding using profiles from T90 guide rails. The system designed to simulate elevator car loads applied during operation of an elevator was for the application of tensile and shear loads of a guide rail unit.

A data acquisition and measurement equipment were used during the experimental studies. Test setup was designed for experimental stress analysis of complete guide rail fastening systems, brackets and fasteners were connected to the T90/B guide rails at the test tower in ITU Faculty of Mechanical Engineering (Figure 4). Available sensors and data acquisition system connected to the guide rail fasteners. Real time data were obtained by examining different loading conditions of the elevator test cabin. Tests were carried out in the test tower which is 7.3 m high. The purpose of the tests were to investigate the forces from the guide rail fasteners and brackets under different loading conditions of elevator cabin and interpret the results as experimentally.



Figure 4. The test tower in ITU Elevator Technology Laboratory

USB sensor interface device is used to transfer data from sensors to the PC environment (DigiVision Software) (Figure 5). It has 16-bit resolution and allows up to 2500 measurements per second.



Figure 5. Data acquisition and signal processing system of the test setup

Load measurement sensors are divided into two categories; these are tension and compression load cell and donut load cell (Figure 6). In this study donut load cells were used in order to investigate the compression loads on bolts.



Figure 6. Donut type load cell used in experiments

In the test, 8-person elevator cabin with empty and loaded (100% full) cases were investigated. Steel casting weights, each weighing 17.3 kgs, were used in the elevator cabin frame to ensure empty and full status (Figure 7).



Figure 7. Elevator test car loading conditions

Brackets elements, made of St37 material, and were utilized at the test tower. Test results were taken from the ring type (donut) load cells placed on guide rail fasteners (steel clips) (Figure 8). During test car's course, the forces applied on the brackets and the bracket joints were observed through donut load cells.



Figure 8. Donut type load cell used in experiments

In tests T90/B type standard guide rail was used. Guide rails were fitted to the base with four bearings and there is 2000 mm distance between the guide rail mounting brackets. Different test cases and configurations can be seen on Figure 9.

Bolts were fastened by different torques. These torques caused 3 different preloading conditions: 2000, 2500, 3000 N. Point zero calibrated in accordance to these pre-loads. Forces below pre-load values are negative and above these values are positive. Results can be found on section in Table 1 and 2.



Figure 9. Configurations of 3 different test cases

4. TEST RESULTS AND CONCLUSION

The matter of seismic activities on the elevator systems is not a new discussion but it has come into question especially after Van Earthquake 2011 in Turkey. The improved safety aspect must be underlined in respect to structural safety and reliability during seismic activities. So this paper focused on seismic activity loads and their effects on guide rail fasteners. Thus brackets and bolts were subjected to loads similar to the case of seismic activities.

As can be seen in Table 1 and Table 2, maximum load occurred on bolts is -470.6 N at Test-3 in 3000 N pre-load condition from C1 load cell. According to Eq.1 the force to untie this connection must be more than 7549~8088 N due to the standards (BS EN ISO 898-1:1999). Comparison of these two values shows that safety factor is approximately 16.

Load Cell	Pre Loaded	Test-1		Test-2		Test-3	
		Min	Max	Min	Max	Min	Max
C1	2000	-47.3	42.4	-28.6	75.9	-91.1	42.0
	2500	-58.5	38.4	-77.3	13.4	-131.8	37.9
	3000	-63.0	113.9	-102.3	-11.1	-59.4	78.6
C2	2000	-105.2	91.4	-192.2	3.1	-162.8	70.0
	2500	-120.4	79.4	-135.1	71.8	-197.5	57.5
	3000	-180.2	41.5	-106.6	97.7	-110.6	142.3

Table 1. Forces occurred on the bolts in empty car case [N]

Table 2. Forces occurred on the bolts in loaded car case [N]

Load Cell	Pre Loaded	Test-1		Test-2		Test-3	
		Min	Max	Min	Max	Min	Max
C1	2000	-332.0	78.6	-179.2	94.3	-43.8	208.2
	2500	-186.3	103.2	-339.6	127.3	-133.6	221.2
	3000	-223.4	55.4	-292.7	4.4	-470.6	172.0
C2	2000	-229.2	72.2	-135.1	127.1	-68.7	179.3
	2500	-230.5	55.3	-186.0	125.8	-75.4	189.1
	3000	-197.1	168.1	-116.8	151.2	-169.9	111.9

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BIOGRAPHICAL DETAIL

Sühan ATAY Mr. Atay received the BSc degree in Mechanical Engineering from ITU in 1995 and MSc degree in Mechanical Design from ITU in 2013. He is working as a Design Engineer.

Eren KAYAOĞLU has been employed as a research assistant in ITU since 2007. Mr. Kayaoğlu received the BSc degree in Mechanical Engineering from Yıldız Technical University in 2004 and MSc degree in Mechanical Design from ITU in 2009. He has carried out research into PhD thesis. He started to work in a project on Wire Rope Isolators (WRI). He is also a Member of Chamber of Mechanical Engineers in Istanbul, Turkey

Adem CANDAŞ has been employed as a research assistant in ITU. Mr. Candas received the BSc degree in Mechanical Engineering from ITU in 2010 and MSc degree in Mechanical Design from ITU in 2009 carried out research into PhD thesis.

C.Erdem IMRAK has been employed as a fulltime Professor in ITU. Prof. Imrak received the BSc, MSc, and PhD degrees in Mechanical Engineering from ITU in 1990, 1992 and 1996 respectively. He has carried out research into materials handling and especially lift systems. Currently his activities include: a Member of the IAEE; a Member of the OIPEEC, a Member of Chamber of Mechanical Engineers in Turkey; a Member of Steering & Consulting Committee of Asansör Dunyası Magazine and a Member of International Committee of Elevatori and Rapporteur from Turkey.

Sefa TARGIT graduated from the Division of Industrial Engineering, Faculty of Mechanical Engineering at ITU. After graduation in 1982, he worked as the mechanical installations engineer in various construction companies and in 1992, he joined ASRAY and thus, the manufacturers side of the Lift Industry. He is currently a partner and the General Manager of ASRAY; Vice President of AYSAD (Turkish Elevator and Escalator Association); Board member of SEDEFED (Federation of Industrial Associations of Turkey). He is a member of the Board of Adviser in ITU, Faculty of Mechanical Engineering, Lift Technical Committee of Ministry of Industry; ELA Component Committee; MMO Turkey (Chamber of Mechanical Engineers), IAEE. He is a publishing advisor of the "Asansör Dünyası" Magazine published in Turkey.

Yusuf Z. KOCABAL has been employed as a lecturer in ITU since 1984. Mr. Kocabal received the BSc degree in Technical Education from Marmara University. He is also the chairman of the sport committee and the chief executive lecturer of technical drawing lessons in ITU Faculty of Mechanical Engineering.