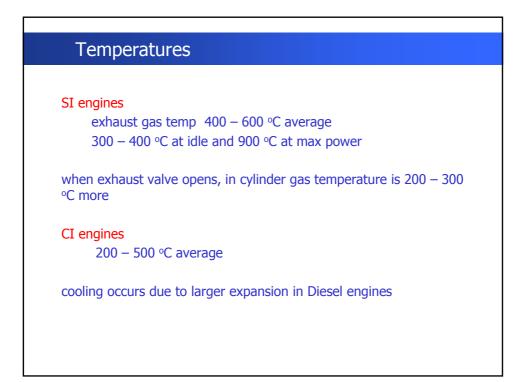
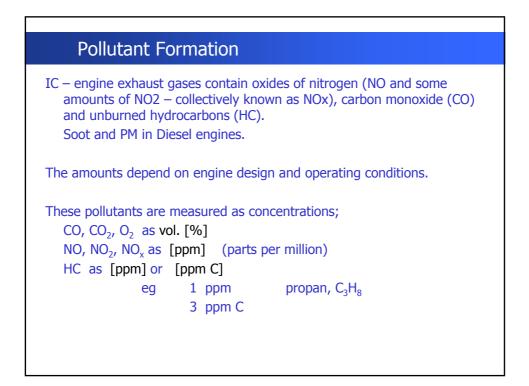
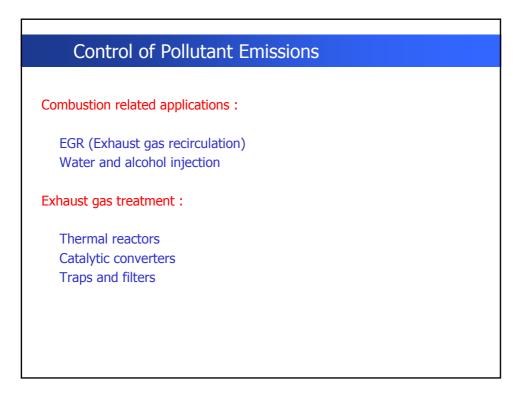
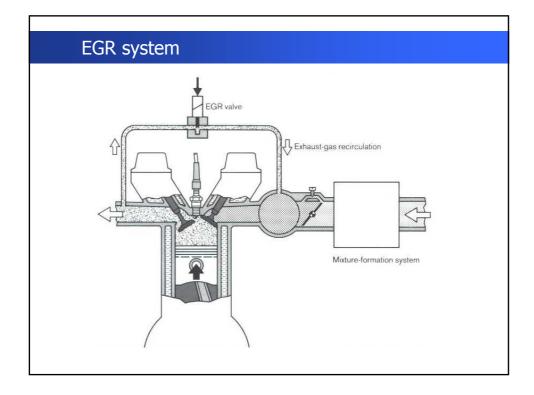


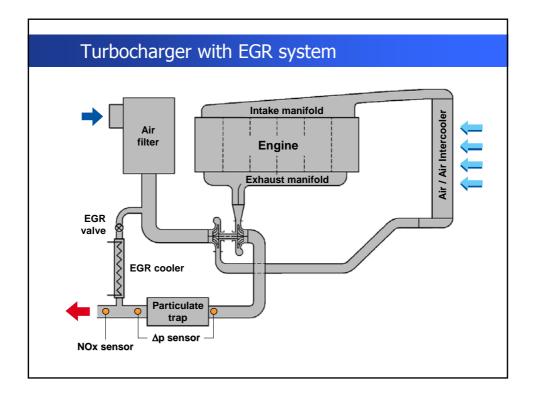
Introduction
Displacement phase (exhaust stroke) mass flow is controled by piston movement from BDC to TDC pressure is slightly above atm pressure
closing of the valve starts at or close to TDC and the total closing is at 8 $-$ 50 $^{\rm o}$ ATDC
Valve overlap intake valve starts to open 10 – 25 ° BTDC valve overlap 15 – 50 ° CA
there can be reverse flow into cylinder : inc residual gases, which is worst at low speeds and idle short circuit of intake air/fuel mixture – inc pollution

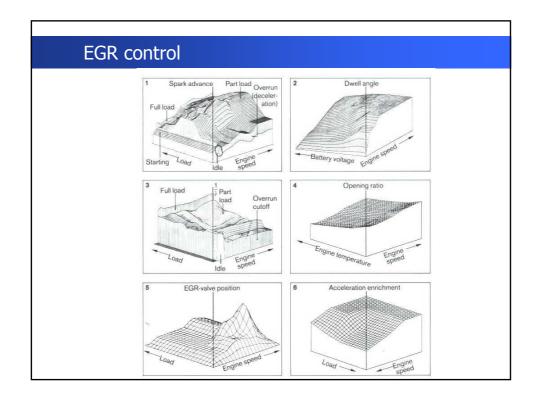






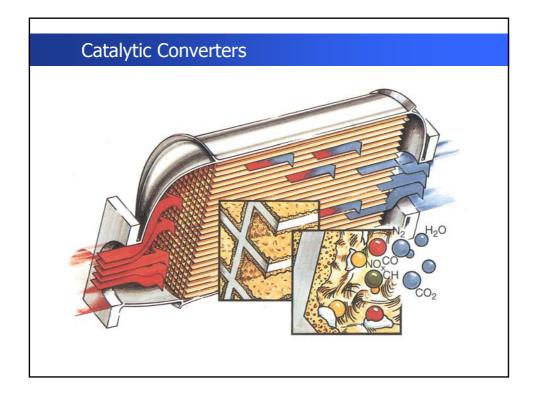




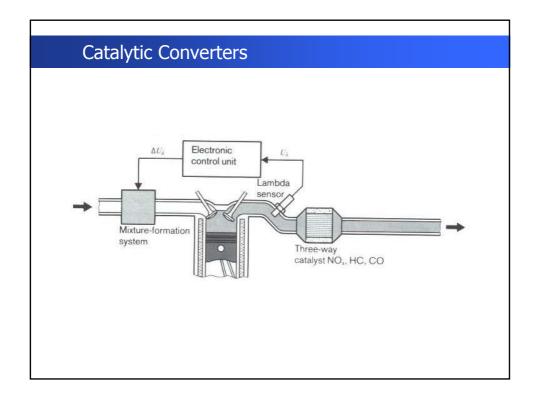


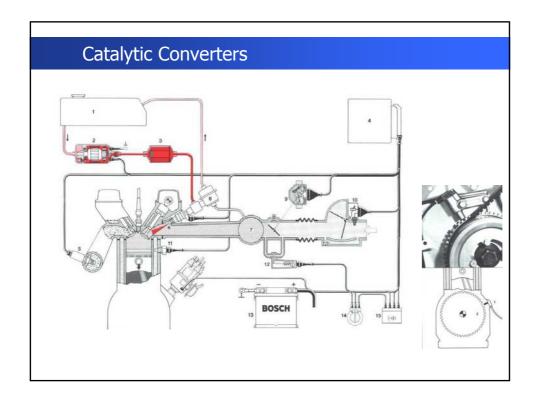
Exhaust Gas Treatment					
Thermal read	tors				
Require	high temperatures,				
	oxygen availability,				
	sufficient time for reactions.				
Used for o	xidation of CO and HC				
Rich mixtu	re + O2 supplement : CO oxidation in exhaust system				
	T, but fuel consumption also increases.				
Lean mixtu	ure + late ignition : high exhaust temperatures, but loss in				
power out					

Exhaust Gas Treatment Catalytic converters Oxidizing catalysts for HC and CO Reducing catalysts for NOx Three-way catalysys for all three pollutants



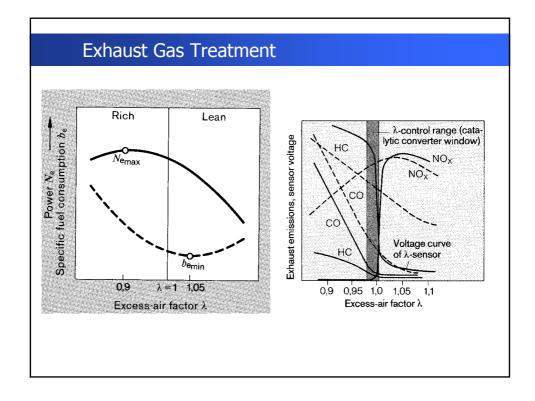


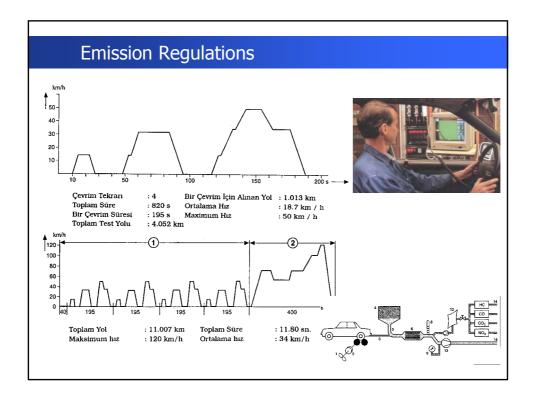


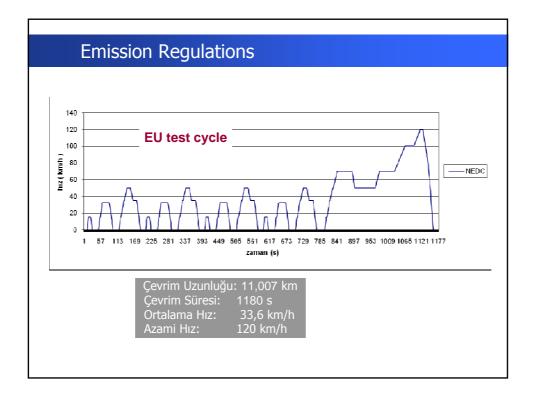


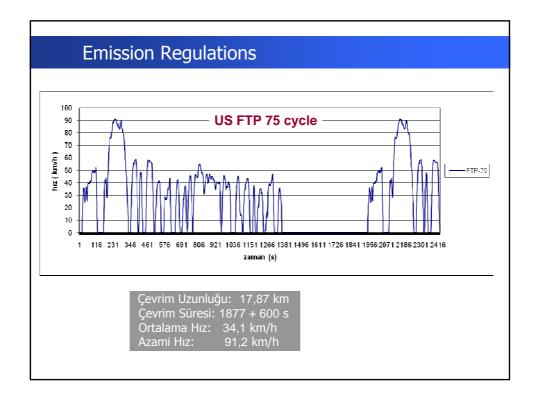
Exhaust Gas Treatment	
$C_mH_n + [m+n/4] O_2 \rightarrow m CO_2 + n/2 H_2O$	(1)
$CO + \frac{1}{2}O_2 \rightarrow CO_2$	(2)
$H_2 + \frac{1}{2} O_2 \rightarrow H_2 O$	(3)
$\text{CO} + \text{NO} \rightarrow \frac{1}{2} \text{N}_2 + \text{CO}_2$	(4)
$C_mH_n + 2 [m+n/4] \text{ NO } \rightarrow [m+n/4] \text{ N}_2 + n/2 \text{ H}_2\text{O} + m \text{ CO}_2$	(5)
$H_2 + NO \rightarrow \frac{1}{2} N_2 + H_2O$	(6)
$SO_2 + \frac{1}{2}O_2 \rightarrow SO_3$	(7)
$5/2 H_2 + NO \rightarrow NH_3 + H_2O$	(8)
$SO_2 + 3 H_2 \rightarrow H_2S + 2 H_2O$	(9)
$NH_3 + CH_4 \rightarrow HCN + 3 H_2$	(10)
$CO + H_2O \rightarrow CO_2 + H_2$	(11)
$CH_n + 2H_2O \rightarrow CO_2 + [2+n/2]H_2$	(12)

Exhaust Gas Treatment	
$\begin{array}{l} \text{CO} + \frac{1}{2} \text{ O}_2 \rightarrow \text{CO}_2 \\ \text{CO} + \text{NO} \rightarrow \frac{1}{2} \text{ N}_2 + \text{CO}_2 \\ \text{In lean mixtures reaction (2) is dominant - O2 is prese \\ \text{CO is reduced by oxidation and insufficient CO for the reaction(4).} \end{array}$	
CO + H ₂ O → CO ₂ + H ₂ CH _n + 2 H ₂ O → CO ₂ + [2+n/2] H ₂ In rich mixtures reactions (11) and (12) have to be fas	(11) (12) ter.

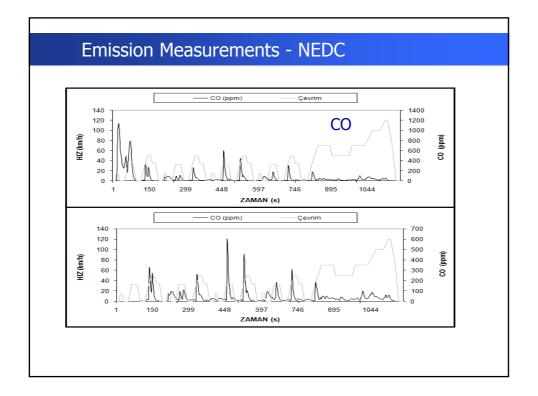


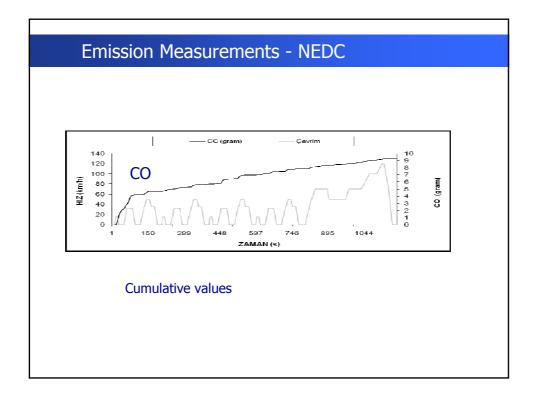


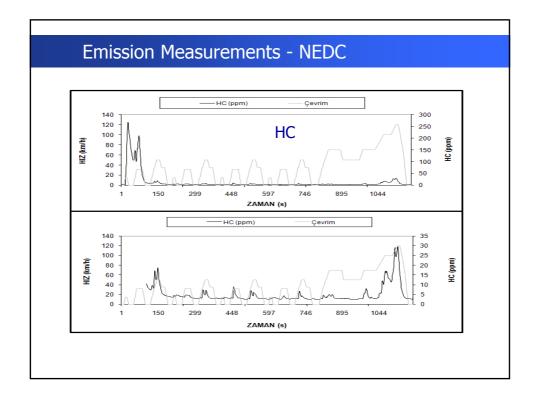


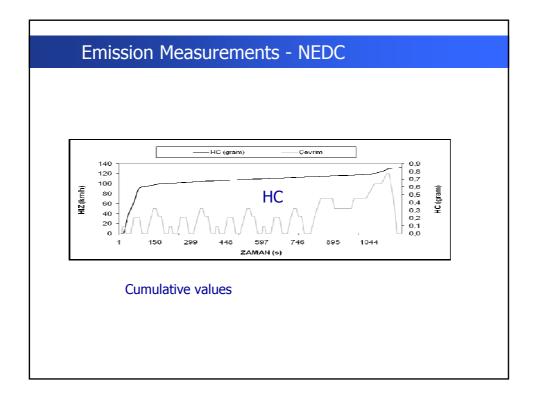


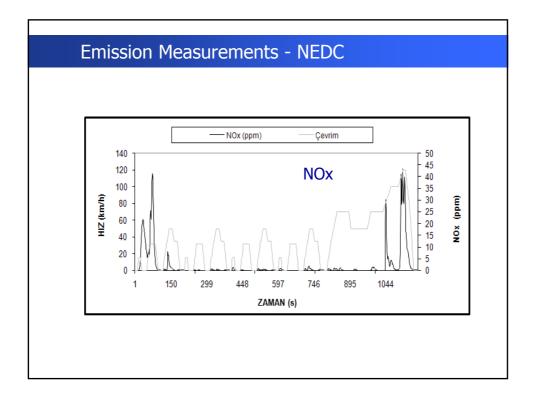


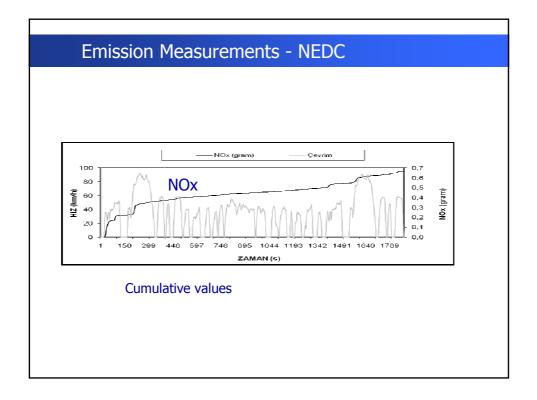


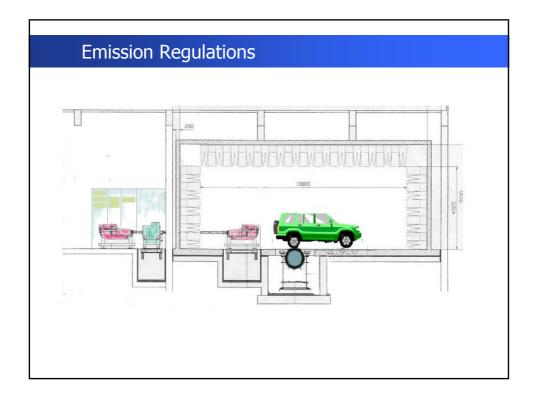


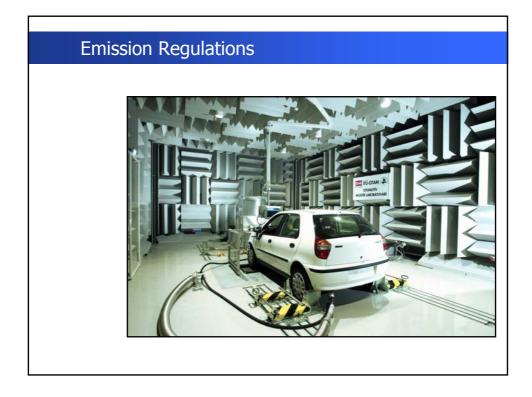




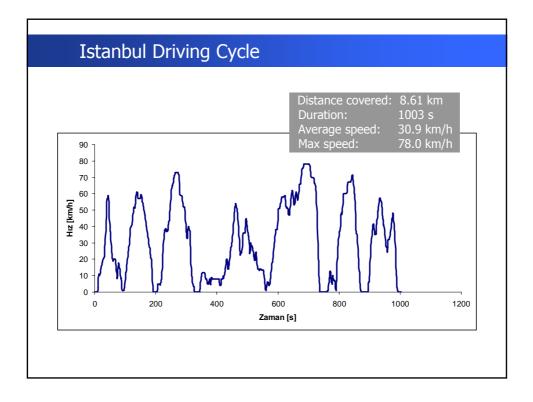












	, 						
	FTP 75		NEDC		IDC (**)		IPCC
	CO2	Fuel	CO2	Fuel	CO2	Fuel	CO2
	[g/km]	Cons.	[g/km]	Cons.	[g/km]	Cons.	[g/km]
		[l /100km]		[l /100km]		[l /100km]	
UC ^(*)	149.5	7.9	169.1	8.6	160.8	8.9	270
R15.04	139.2	6.8	166.1	7.8	166.1	8.2	200
EURO1	134.8	6.0	169.5	7.5	180.2	8.1	200
EURO3	133.3	5.9	155.4	6.9	159.6	7.2	205
EURO4	144.9	6.2	153.6	6.5	164.7	7.1	205

Source: Soruşbay, C., Binek Araçlarında Sürüş Koşullarının Kirletici Egzoz Emisyonlarına Etkisi, IV. Ulusal Hava Kirliliği ve Kontrolü Semp, HKK2010, ODTÜ, Ankara, 2010.