

# Circuit and System Analysis

## EEF 232E

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# Outline I

- Transfer function Continue
- Kirchhoff's Laws in the Frequency Domain
- The Passive Circuit Elements in the Frequency Domain
- The Concept of Impedance and Admittance
- Resonance

# Transfer function

$$H(j\omega) \in \mathbb{C}$$

$$H(j\omega) = |H(j\omega)|e^{j\angle H(j\omega)}$$

$$U(j\omega) \in \mathbb{C}$$

$$U(j\omega) = |U(j\omega)|e^{j\angle U(j\omega)}$$

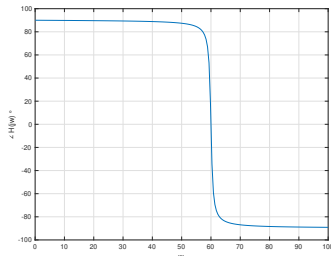
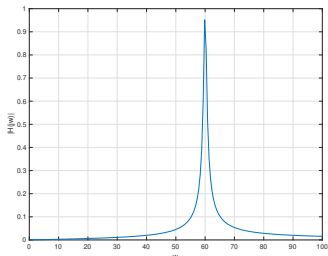
$$\begin{aligned} Y(j\omega) &= H(j\omega)U(j\omega) = |H(j\omega)|e^{j\angle H(j\omega)}|U(j\omega)|e^{j\angle U(j\omega)} \\ &= |H(j\omega)||U|e^{j(\angle H(j\omega)+\angle U)} \end{aligned}$$

$$y(t) = \underbrace{|H(j\omega)||U|}_{|Y(j\omega)|} \cos(\omega t + \underbrace{\angle H(j\omega) + \angle U}_{\angle Y(j\omega)})$$

# Transfer function

$$H(j\omega) = \frac{j\omega/Q}{(j\omega)^2 + j\omega/Q + \omega_0^2}$$

```
>>Q=1;w0 = 60;%Matlabcode  
>>w = linspace(0.1,100,200);  
>>H=(j*w./Q)./((j*w).^2 + j * w./Q + w0^2);  
>>plot(w,abs(H));plot(w,unwrap(angle(H))*180/pi);
```



$w = 60; |H| = 1; \angle = 0^\circ$  and  $w = 40; |H| = 0.02; \angle = 88.8542^\circ$

# Kirchhoff's Laws in the Frequency Domain: KVL

Lets assuming that  $v_1, v_2 \dots v_{n_e}$ , represent voltages around a closed path in a circuit.

KVL requires that

$$\sum_{k=1}^{n_e} v_k(t) = 0$$

We assume that the circuit is operating in a sinusoidal steady state therefore

$$\sum_{k=1}^{n_e} \Re \{ V_k e^{j\omega t} \} = 0$$

Factoring the term  $e^{j\omega t}$  from each term yields

$$\sum_{k=1}^{n_e} V_k = 0.$$

# Kirchhoff's Laws in the Frequency Domain: KCL

A similar derivation applies to a set of sinusoidal currents (KCL). Thus if

$$\sum_{k=1}^{n_e} i_k(t) = 0$$

We assume that the circuit is operating in a sinusoidal steady state therefore

$$\sum_{k=1}^{n_e} \Re\{I_k e^{j\theta_k}\} = 0$$

Factoring the term  $e^{j\omega t}$  from each term yields

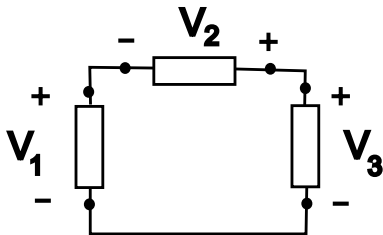
$$\sum_{k=1}^{n_e} I_k = 0.$$

**Question 1:** Four branches terminates at a common node. The reference direction of each branch current ( $i_1, i_2, i_3, i_4$ , is toward the node if

$$i_1 = 100 \cos(\omega t + 25^\circ) \text{A} \quad i_2 = 100 \cos(\omega t + 145^\circ) \text{A}$$

$$i_3 = 100 \cos(\omega t - 95^\circ) \text{A}, \text{ find } i_4$$

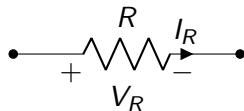
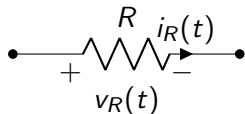
**Question 2:**



$$v_1(t) = 100 \cos(\omega t + 30^\circ) \text{V} \quad v_2(t) = 100 \sin(\omega t + 45^\circ) \text{V}, \text{ find } v_3(t)$$

# The Passive Circuit Elements in the Frequency Domain

## Resistors



From Ohm's law, if the current in a resistor varies sinusoidally with time, the voltage at the terminals of the resistor

$$v(t) = R \Re\{I_R e^{j\omega t}\} = \Re\{R I_R e^{j\omega t}\}$$

$$\Re\{V_R e^{j\omega t}\} = \Re\{R I_R e^{j\omega t}\}$$

from the properties of phasor

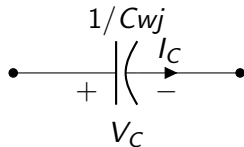
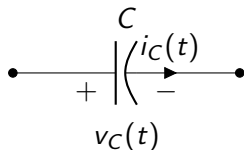
$$V_R = R I_R \text{ or } I_R = G V_R$$

There is no phase shift between the current and voltage of resistor. The signals of voltage and current are said to be in phase.



# The Passive Circuit Elements in the Frequency Domain

## Capacitor



Substituting the phasor representation of the current and phasor voltage at the terminals of a capacitor into  $i = C \frac{dv}{dt}$

$$\Re\{I_C e^{j\omega t}\} = C \frac{d\Re\{V_C e^{j\omega t}\}}{dt}$$

using the properties of phasor

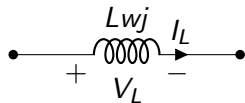
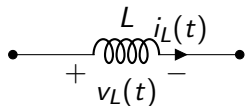
$$\Re\{I_C e^{j\omega t}\} = \Re\left\{C V_C \frac{de^{j\omega t}}{dt}\right\} = \Re\{C j\omega V_C e^{j\omega t}\}$$

we get

$$I_C = j\omega C V_C$$

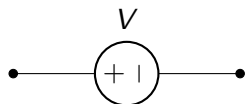
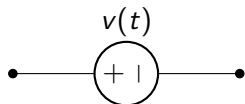
# The Passive Circuit Elements in the Frequency Domain

## Inductor

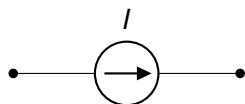
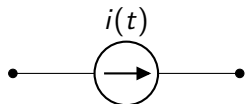


$$V_L = j\omega L I_L$$

## Independent voltage sources



## Independent current sources



$$I = I_m e^{j\theta} \text{ and } V = V_m e^{j\theta}$$

# The Passive Circuit Elements in the Frequency Domain

$$I_C = j\omega CV_C = \omega CV_C e^{j\frac{\pi}{2}}$$

$$\angle I_C = \angle V_C + \frac{\pi}{2}$$

The current leads the voltage across the terminals of a capacitor by  $90^\circ$ .

$$V_L = j\omega L = \omega L I_L e^{j\frac{\pi}{2}}$$

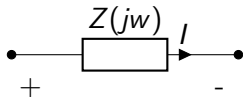
$$\angle V_L = \angle I_L + \frac{\pi}{2}$$

The current lags the voltage by  $90^\circ$ .

# The Concept of Impedance and Admittance

The driving-point impedance of the one-port at the frequency  $\omega$  to be the ratio of the port-voltage phasor  $V$  and the input-current phasor  $I$  that is,

$$Z(j\omega) = \frac{V}{I}.$$



$Z$  represents the **impedance** of the circuit element

$$Z = \frac{V}{I} = R + jX$$

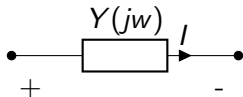
$R$ , is called resistance and  $X$ , is called reactance.

Note

$$Z = \frac{V}{I} = \frac{1}{Y}$$

# The Concept of Impedance and Admittance

$$Y(j\omega) = \frac{I}{V}.$$

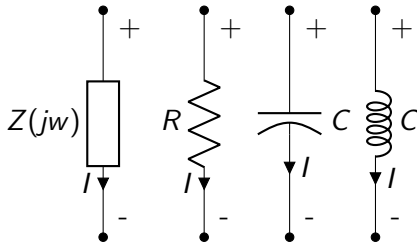


$Y$  represents the **admittance** of the circuit element

$$Y = \frac{V}{I} = G + jB$$

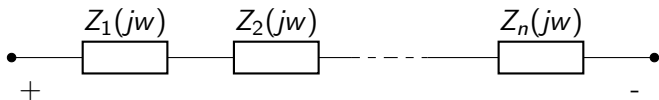
$G$ , is called conductance and  $B$ , is called susceptance.

Element	Impedance	Reactance	Admittance	Susceptance
Resistor	$R$	$-$	$G$	$-$
Capacitor	$-j/\omega C$	$-1/\omega C$	$j\omega C$	$\omega C$
Inductor	$j\omega L$	$\omega L$	$-j/\omega L$	$-1/\omega L$



Lets  $Z = |Z|e^{j\theta}$  if  $\theta < 0$ , this impedance is Capacitive if  $\theta > 0$  this impedance is Inductive !

# Combining Impedance in Series and Parallel



Impedances in series can be combined into a single impedance by simply adding the individual impedances.

$$Z = Z_1 + Z_2 + \dots + Z_n$$

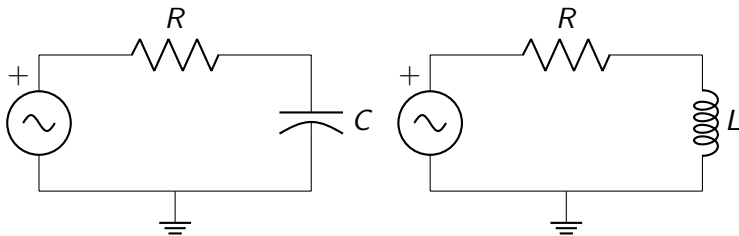
when they in parallel

$$Z = \left\{ \frac{1}{Z_1} + \frac{1}{Z_2} + \dots + \frac{1}{Z_n} \right\}^{-1}$$

admittances in parallel:

$$Y = Y_1 + Y_2 + \dots + Y_n$$

# RC and RL Circuits



$$I_C = \frac{V_s}{1 + CRj\omega}, \quad I_L = \frac{V_s}{R + Lj\omega}$$

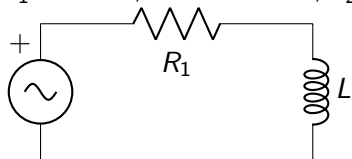
See: [Circuits>A/C Circuits>Caps of Various Capacitances](#); Also :

[Circuits>A/C Circuits>Caps w/ of Various Frequencies](#); [Circuits>A/C Circuits>Inductors of Various Inductances](#);

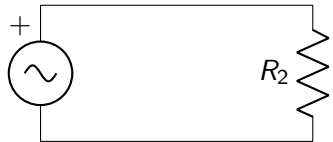
[Circuits>A/C Circuits>Inductors w/ of Various Frequencies](#)



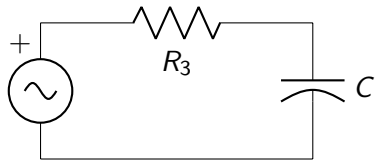
$R_1 = 100\Omega$ ;  $L = 344.6mH$ ;  $R_2 = 200\Omega$ ;  $R_3 = 100\Omega$ ;  $C = 11.5\mu F$ ;  $f = 80Hz$



$$Z_1 = R_1 + Lj\omega = 200e^{j60^\circ} \Omega$$



$$Z_2 = R_2 = 200\Omega$$

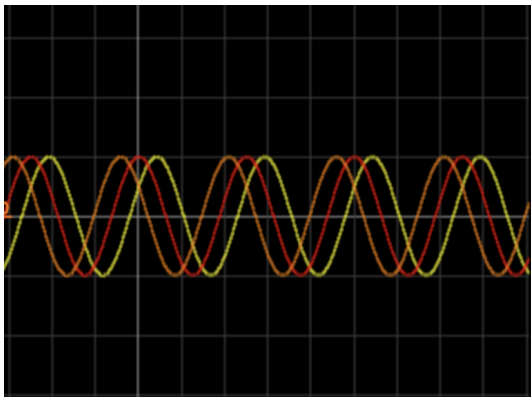


$$Z_3 = R_3 + \frac{1}{Cj\omega} = 200e^{-j60^\circ} \Omega$$

$$|Z_1| = 200, \angle Z_1 = 60^\circ, |Z_2| = 200, \angle Z_2 = 0^\circ, |Z_3| = 200, \angle Z_3 = -60^\circ,$$

Current:

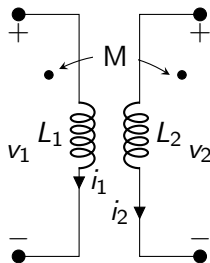
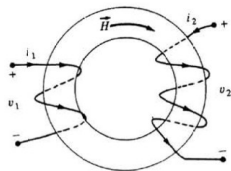
$$I = \frac{V_s}{Z}$$



$$|Z_1| = 200, \angle Z_1 = 60^\circ, |Z_2| = 200, \angle Z_2 = 0^\circ, |Z_3| = 200, \angle Z_3 = -60^\circ,$$

▶ Circuits>A/C Circuits>Caps of Various Capacitances;

# Mutual Inductance

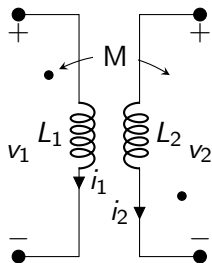


$$\phi_1 = L_1 i_1 + M i_2$$
$$\phi_2 = L_2 i_2 + M i_1$$

$$v_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \quad \rightarrow \quad V_1 = L_1 j\omega I_1 + M j\omega I_2$$

$$v_2 = L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \quad \rightarrow \quad V_2 = L_2 j\omega I_2 + M j\omega I_1$$

# Mutual Inductance



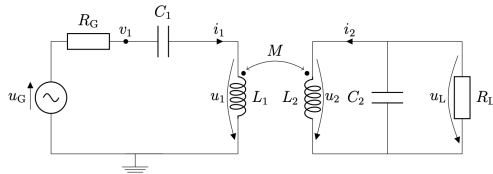
$$\phi_1 = L_1 i_1 - M i_2$$

$$\phi_2 = L_2 i_2 - M i_1$$

and

$$V_1 = L_1 j\omega I_1 - M j\omega I_2$$

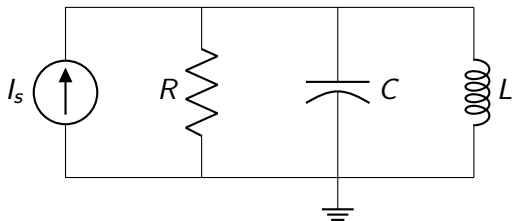
$$V_2 = L_2 j\omega I_2 - M j\omega I_1$$



**Figure 2.1:** Circuit diagram with capacitor  $C_1$  in series with the coil on the primary side. A voltage  $u_G$  is applied to the primary circuit on the left, inducing a voltage  $u_L$  in the secondary circuit on the right.

# Parallel Resonance Circuit

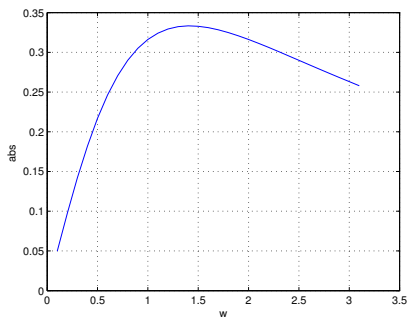
Find the solution for  $R = 1/3\Omega$ ,  $C = 1F$ ,  $L = 1/2H$ ,  $i(t) = \cos(\omega t)$  in SSA.



$$Y_{eq}(j\omega) = \frac{1}{j\omega L} + \frac{1}{R} + j\omega C = \frac{R + j\omega L - \omega^2 RLC}{j\omega RL}$$

$$V_C = Z_{eq}(j\omega) \cdot I_s = \frac{I_s}{Y_{eq}(j\omega)} = \frac{I_s}{\frac{R + j\omega L - \omega^2 RLC}{j\omega RL}} = \frac{j\omega RL}{R - \omega^2 RLC + j\omega L} I_s$$

Magnitude of  $V_C(j\omega)$  is maximum when  $\omega = \frac{1}{\sqrt{LC}}$  !



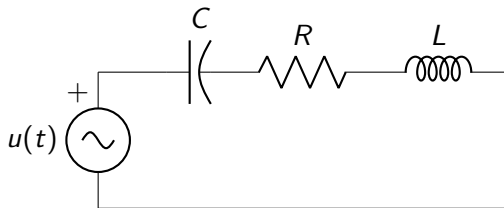
$$Z(j\frac{1}{\sqrt{LC}}) = R$$

## Resonance

Resonance occurs at a particular resonance frequency when the imaginary parts of impedances or admittances of circuit elements cancel each other.

$\omega = \frac{1}{\sqrt{LC}}$  is the resonance frequency.

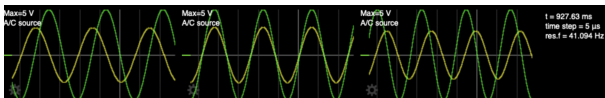
# Serial Resonance Circuit



$$Z = \left( \frac{1}{Cj\omega} + R + Lj\omega \right) = \frac{RC\omega + j(LC\omega^2 - 1)}{C\omega}$$

if  $\omega = \frac{1}{\sqrt{LC}}$  then  $Z = R$ .

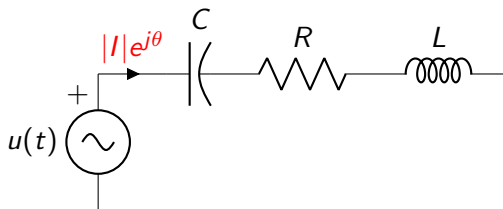
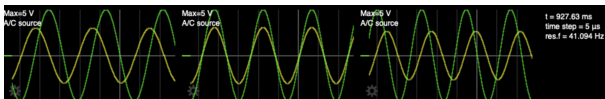
$R = 10, L = 1H$  and  $C = 15\mu F$  then  $\omega_{resonans} = 41Hz$



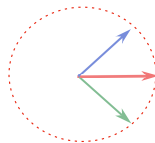
$v_u$  and  $i_u$  for @35Hz, @41Hz and @45Hz

► Circuits > A/C Circuits > Series Resonance

# Serial Resonance Circuit



$$I = \frac{U}{Z} = \frac{|U|}{|Z|e^{j\theta}} = \frac{|U|}{|Z|}e^{-j\theta}$$

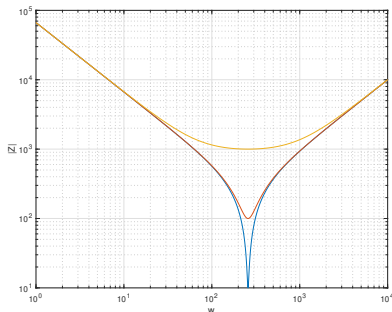
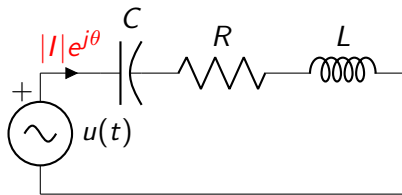




# Serial Resonance Circuit

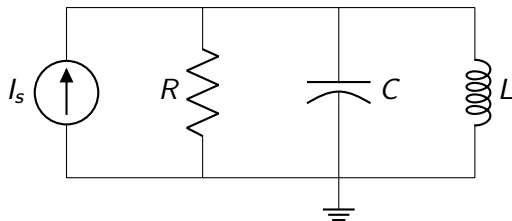
$$V_L = \frac{Lj\omega_0}{Z(\omega_0)} U = \frac{L\omega_0}{R} jU = QjU, \quad V_C = \frac{1}{Cj\omega_0} \frac{1}{Z(\omega_0)} U = -QjU$$

$\omega_0$  resonance frequency and  $Q$  factor at resonance  $Q = \frac{1}{R} \sqrt{\frac{L}{C}}$



$$R = 10\Omega, 100\Omega, 1k\Omega$$

# Parallel Resonance Circuit



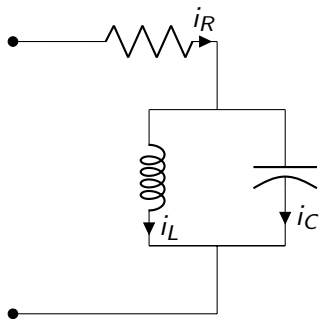
At  $\omega_0$

$$I_C(j\omega_0) = I_s \frac{Cj\omega_0}{Y(j\omega_0)} = I_s \frac{Cj\omega_0}{G} = jI_s Q_p$$

$$I_L(j\omega_0) = I_s \frac{1}{Y(j\omega_0)} \frac{1}{Lj\omega_0} = I_s \frac{R}{Lj\omega_0} = -jI_s Q_p$$

$Q_p$  factor at resonance

## Example



Find the impedance  $Z$  between the terminals:

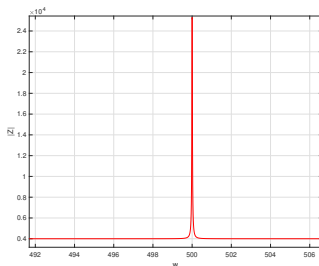
$$Z = R + \left\{ Cj\omega + \frac{1}{Lj\omega} \right\}^{-1} = R + \frac{Lj\omega}{1 - LC\omega^2}$$

$$Z = \frac{R - RLC\omega^2 + Lj\omega}{1 - LC\omega^2}$$

# Example

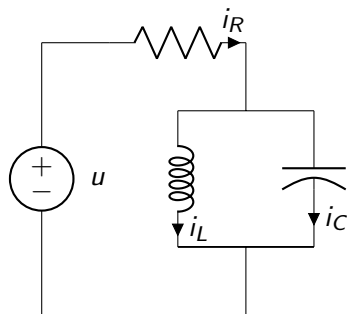
$$Z = \frac{R - RLC\omega^2 + Lj\omega}{1 - LC\omega^2}$$

For  $R = 4k\Omega$ ,  $C = 2mF$  ve  $L = 2mH$



$\omega = \frac{1}{\sqrt{LC}} = 500$  and then  $Z = \frac{***}{0}$  (open-circuit)!

# Example



State equation:

$$\frac{d}{dt} \begin{bmatrix} V_{C1} \\ i_L \end{bmatrix} = \begin{bmatrix} -\frac{1}{RC} & -\frac{1}{C} \\ \frac{1}{L} & 0 \end{bmatrix} \begin{bmatrix} V_{C1} \\ i_L \end{bmatrix} + \begin{bmatrix} \frac{1}{RC} \\ 0 \end{bmatrix} u$$

$$v_R = \begin{bmatrix} -1 & 0 \end{bmatrix} \begin{bmatrix} V_{C1} \\ i_L \end{bmatrix} + u$$

Using the state-equation

$$\begin{aligned} V_C &= [1 \ 0] \begin{bmatrix} j\omega + \frac{1}{RC} & \frac{1}{C} \\ -\frac{1}{L} & j\omega \end{bmatrix}^{-1} \begin{bmatrix} \frac{1}{RC} \\ 0 \end{bmatrix} e \\ &= \frac{\frac{j\omega}{RC}}{\frac{1}{LC} - \omega^2 + \frac{j\omega}{RC}} U \end{aligned}$$

$$\begin{aligned} V_R &= U - V_C = \left\{ 1 - \frac{\frac{j\omega}{RC}}{\frac{1}{LC} - \omega^2 + \frac{j\omega}{RC}} \right\} U \\ &= \left\{ \frac{\frac{1}{LC} - \omega^2}{\frac{1}{LC} - \omega^2 + \frac{j\omega}{RC}} \right\} U \\ &= \frac{R(1 - LC\omega^2)}{Lj\omega + R(1 - LC\omega^2)} U \end{aligned}$$

# Example

Using the The Concept of Impedance, lets find the  $V_R$

$$\begin{aligned}V_R &= R \frac{U}{Z} \\ &= R \frac{(1 - LC\omega^2)}{Lj\omega + R(1 - LC\omega^2)} U\end{aligned}$$

What happen when  $\omega = \frac{1}{\sqrt{LC}}$  ?

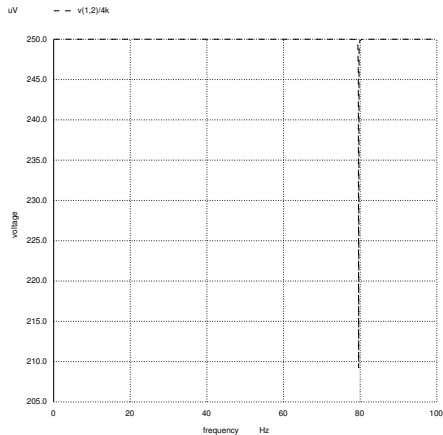
# Example

Sekil 7.2

```
v1 1 0 sin(0 .1 10) dc 0 ac 1
r 1 2 4k
l 2 0 2m
c 2 0 2m
.control
ac lin 1000 .1 100
plot v(1,2)/4k
.endc
.end
```

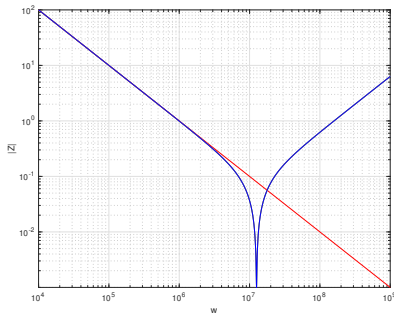
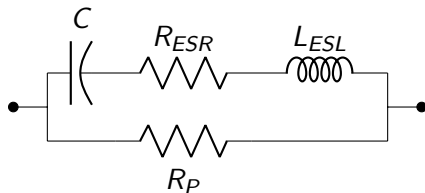


# Example



▶ YouTube Video: Example with two sources

Real Life Problem ! The non-ideal behavior of a capacitor is due to imperfections within the capacitor's material that create resistance causing the capacitor to dissipate energy.



PS:red is ideal...

▶ A producer Web Page (Ceramic Cap (SMD))

$$Z = R_P // \left( \frac{1}{Cj\omega} + R_{ESR} + L_{ESL}j\omega \right)$$

$$C = 10\mu F, R_{ESR} = 1m\Omega, L_{ESL} = 6.33nL, R_P = 100M\Omega.$$