



Finite Element Modeling of Seismic Performance of Low Concrete Strength Exterior Beam-Column Joints

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PRESENTATION OUTLINE

- Introduction
- Beam-Column Joint Test at ITU
- Finite element modeling using DIANA
- Results of Finite Element Analysis
- Conclusions
- Ongoing work at KFUPM

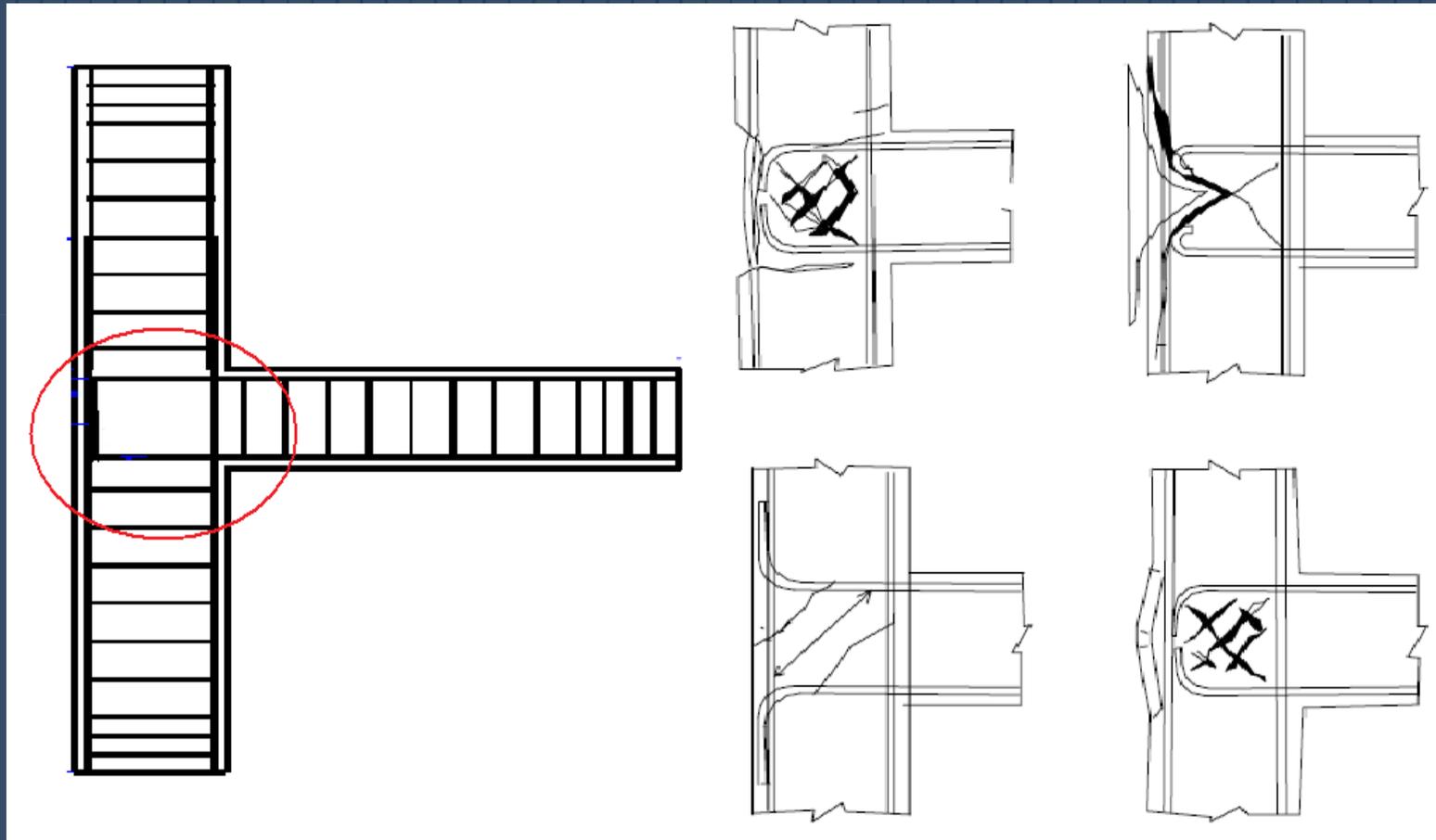
JOINT FAILURE IN BUILDINGS



BACKGROUND

- The Western Region of Saudi Arabia is located in moderately active seismic zone with recent/historical seismic events. Many RC buildings in this region were hitherto designed only for gravity loads using low strength concrete without any ductile detailing of beam-column joints [Alsayed et al]
- An experimental program was conducted at Istanbul Technical University (ITU) on the behavior of exterior beam-column joints subjected to seismic loads. These joints were made with very low strength concrete to simulate the concrete used in reinforced concrete structures in Turkey prior to 1990's. [Bedirhanoglu et al, A. Ilki et al]

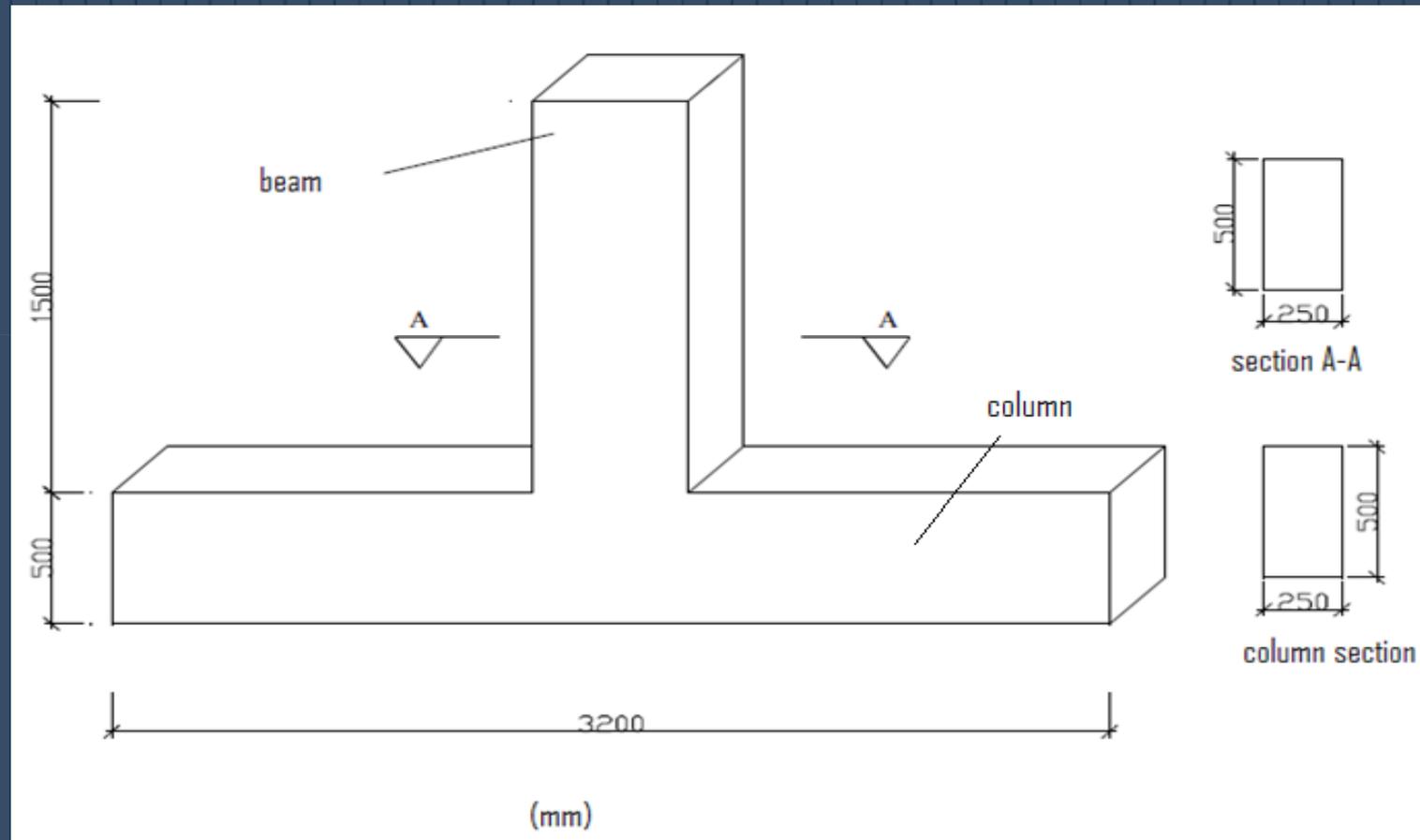
PRE-1990'S DETAILING OF BEAM-COLUMN JOINTS



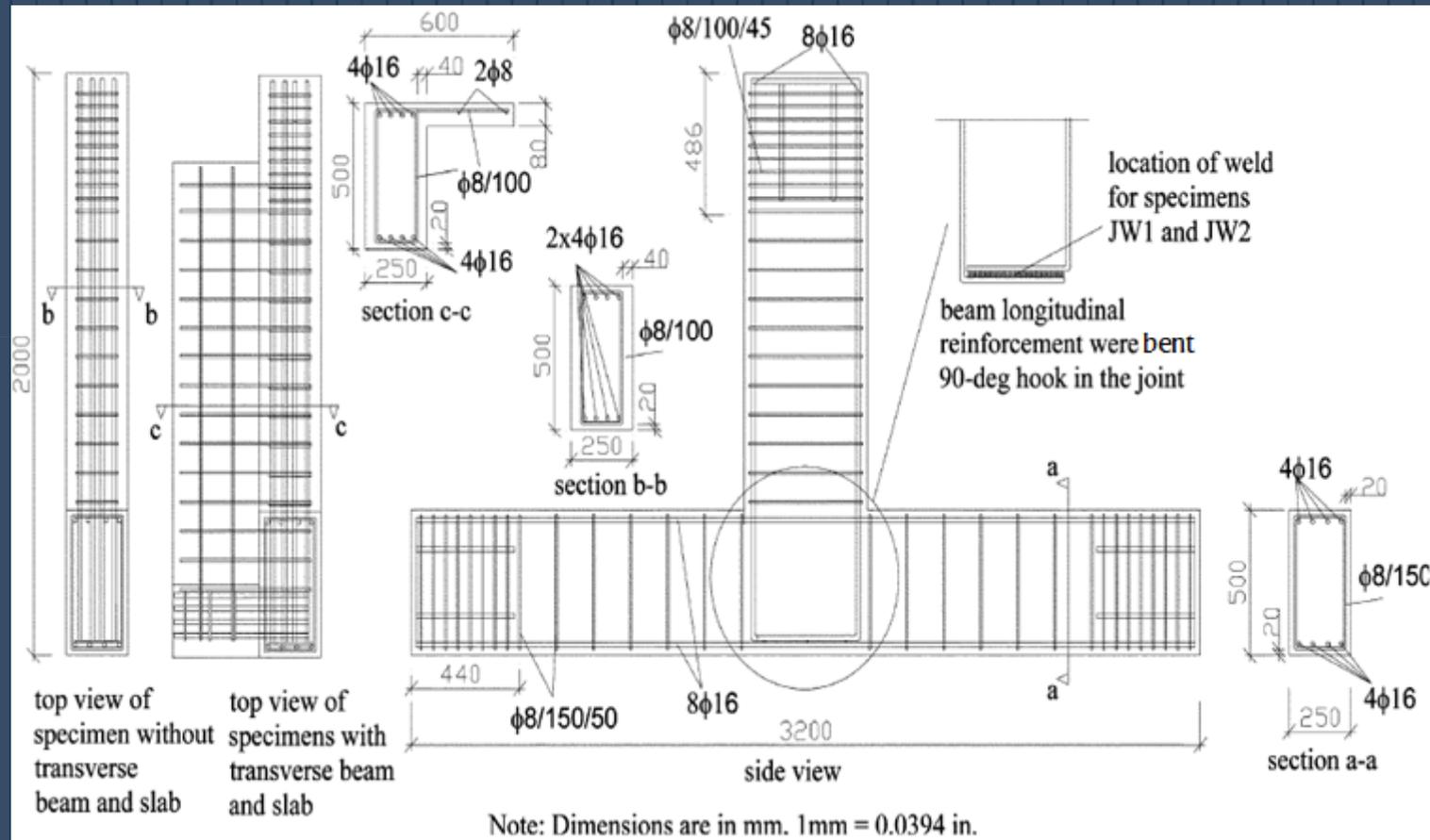
BEAM-COLUMN JOINT TEST AT ITU



GEOMETRY AND REINFORCEMENT DETAILS OF ITU SPECIMEN



GEOMETRY AND REINFORCEMENT DETAILS OF ITU SPECIMEN



MATERIAL PROPERTIES

Mechanical properties of reinforcing bars:

Reinforcement t	Dia(mm)	Fy (Mpa)	ϵ_y	Fs max (Mpa)	ϵ_{smax}
Φ16	16	333	0.0017	470	0.2
Φ8	8	315	0.0016	433	0.2

Material properties of concrete:

f'_c (Mpa)	E_c (Mpa)
8.3	13000

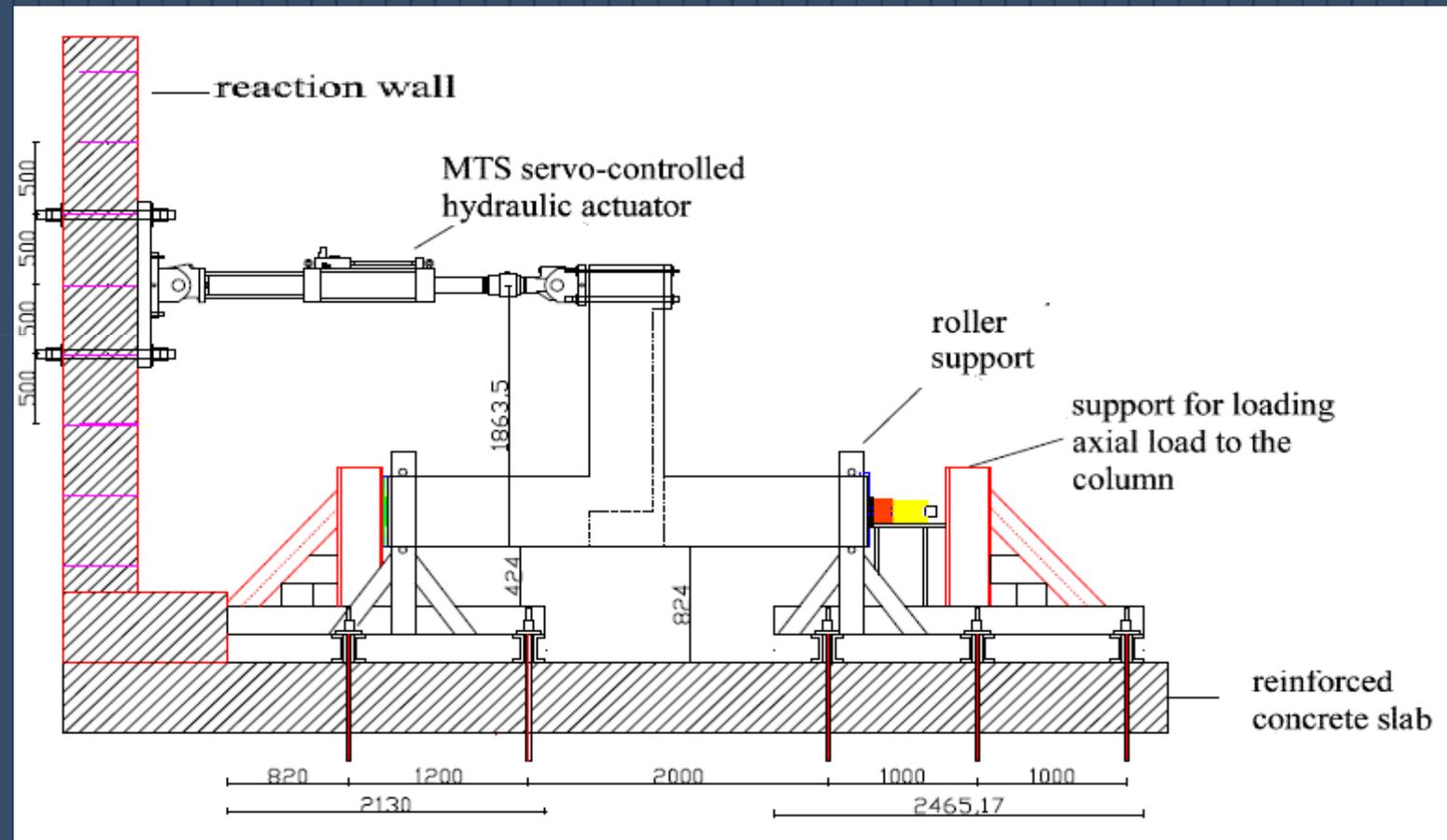
f'_c : low strength concrete

SPECIMEN TESTED AT ITU

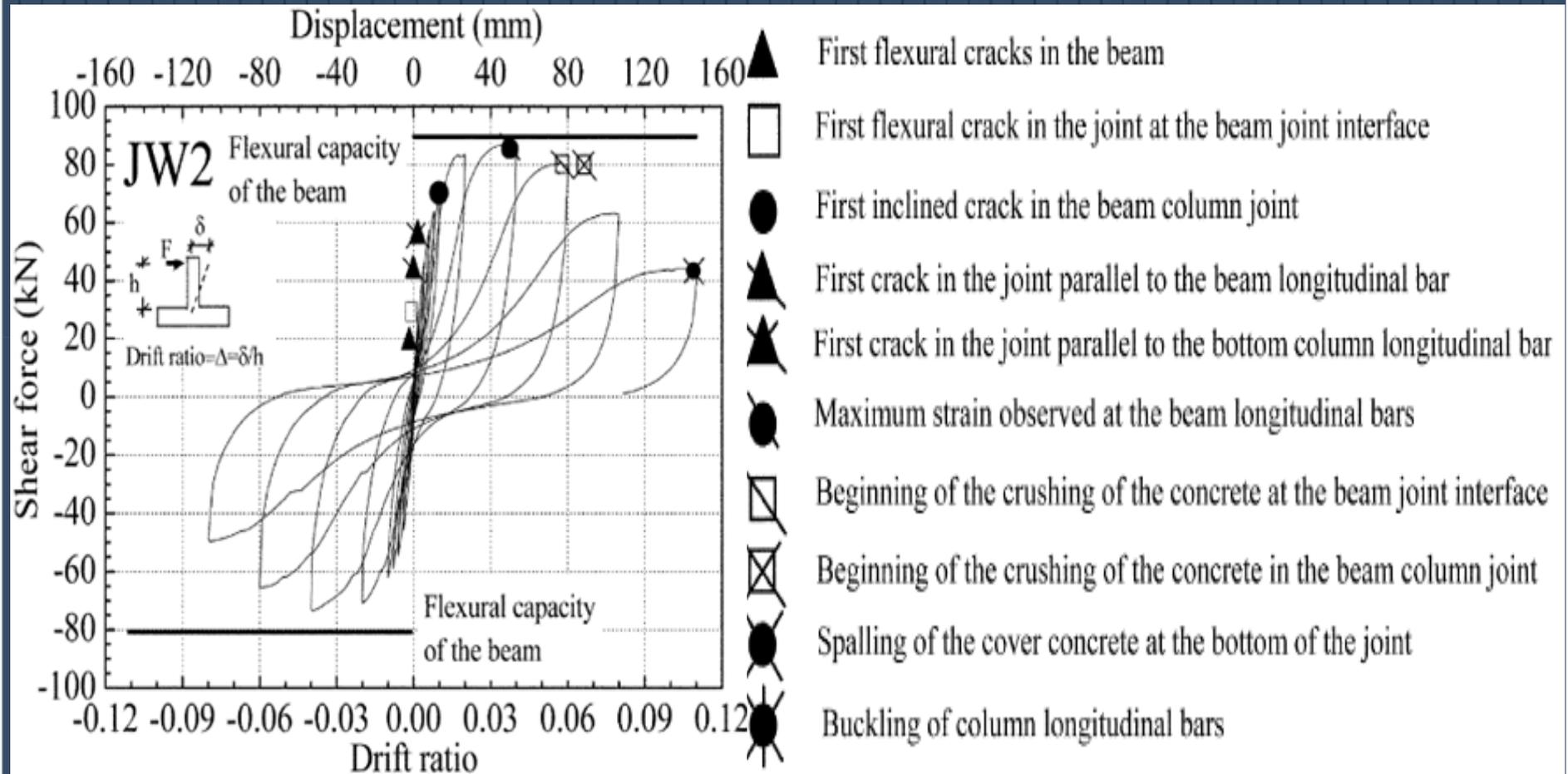
No.	Specimen	Age, days	f'_c , MPa	Joint reinforcement	Transverse beam and slab	Welding of hooks of beam's longitudinal bars at its anchorage in the joint
1	JO1	164	8.3	No	Present	Absent
2	JO2	171	8.3	1 ϕ 8	Present	Absent
3	JO3	179	8.3	4 ϕ 8	Present	Absent
4	JO4	143	8.3	No	Present	Absent
5	JO5	156	8.3	No	Absent	Absent
6	JO6	176	8.3	No	Present	Absent
7	JO7	197	8.3	No	Present	Absent
8	JW1	208	8.3	No	Present	Present
9	JW2	230	8.3	No	Present	Present

- Test specimens selected for F.E modeling are JW1 and JW2 which are with welded hooks and repaired joints with high strength mortar.

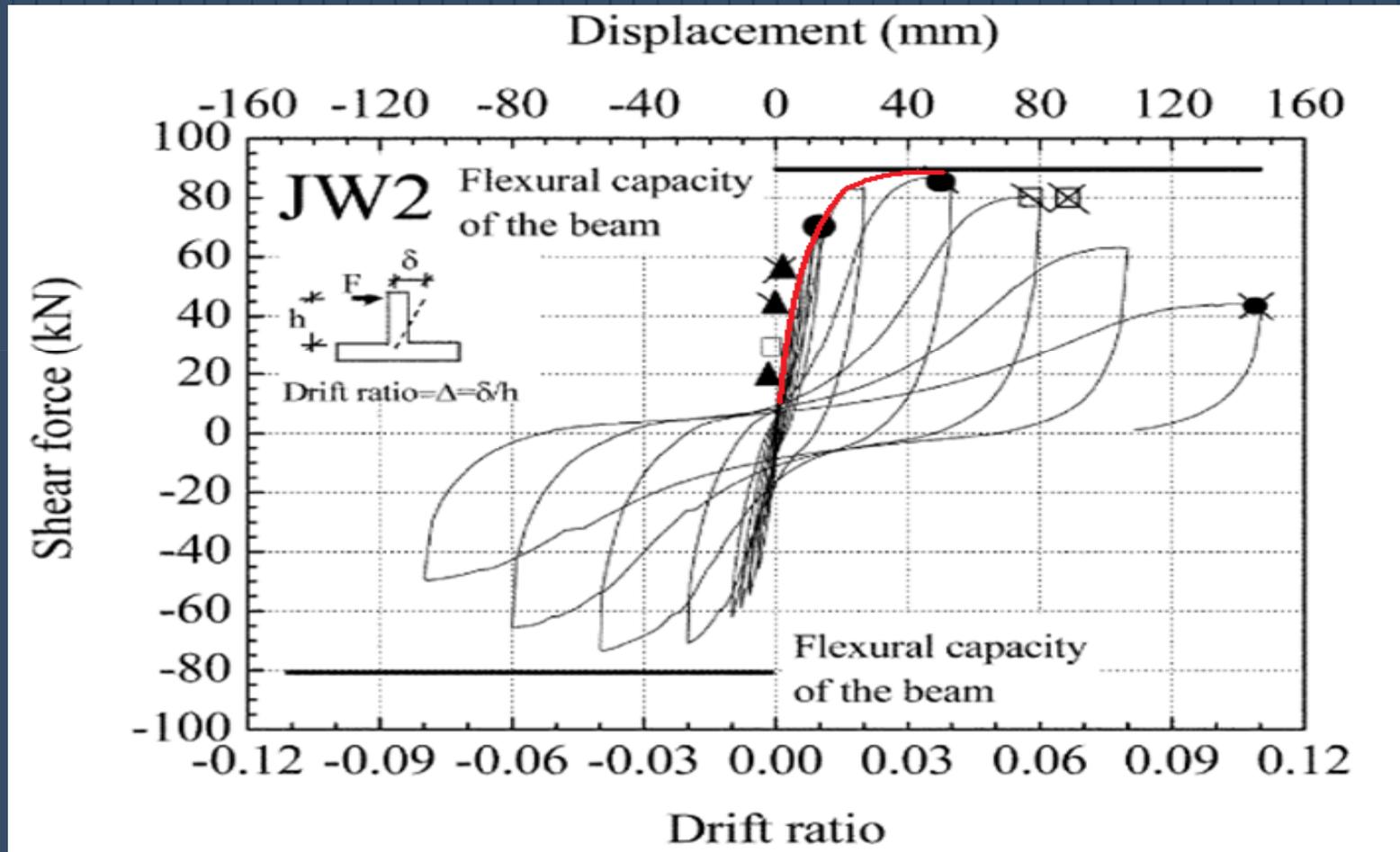
TEST SETUP



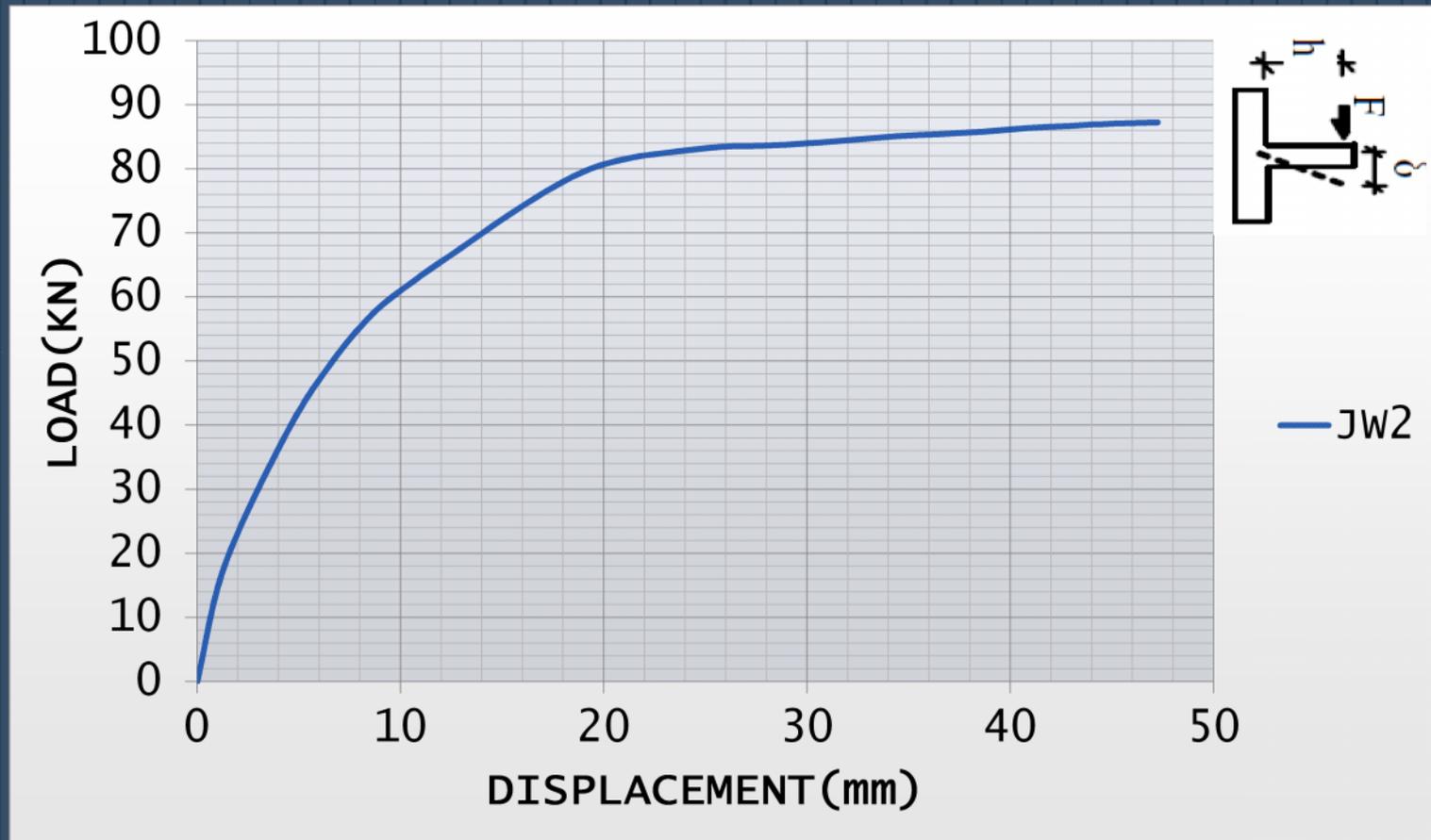
TEST RESULTS FOR JOINT JW2



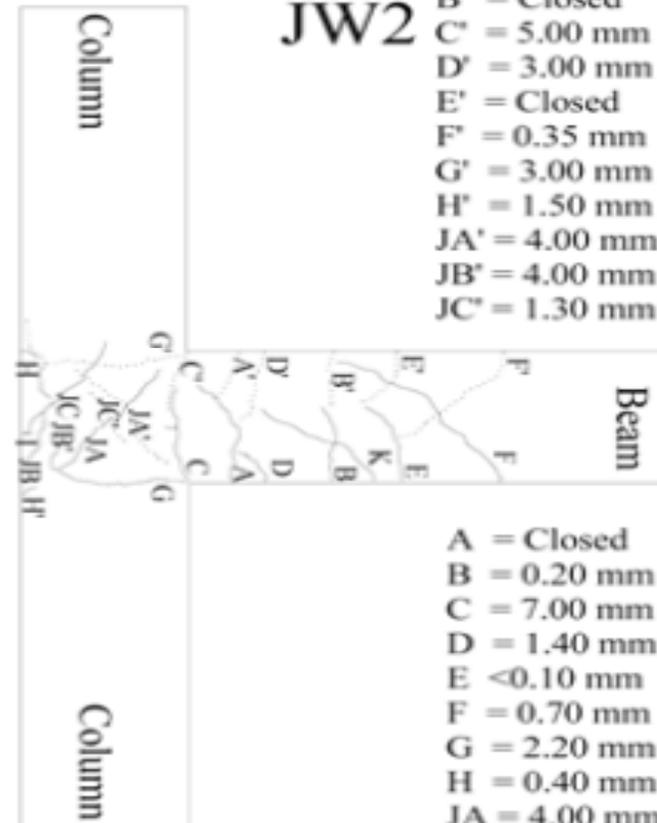
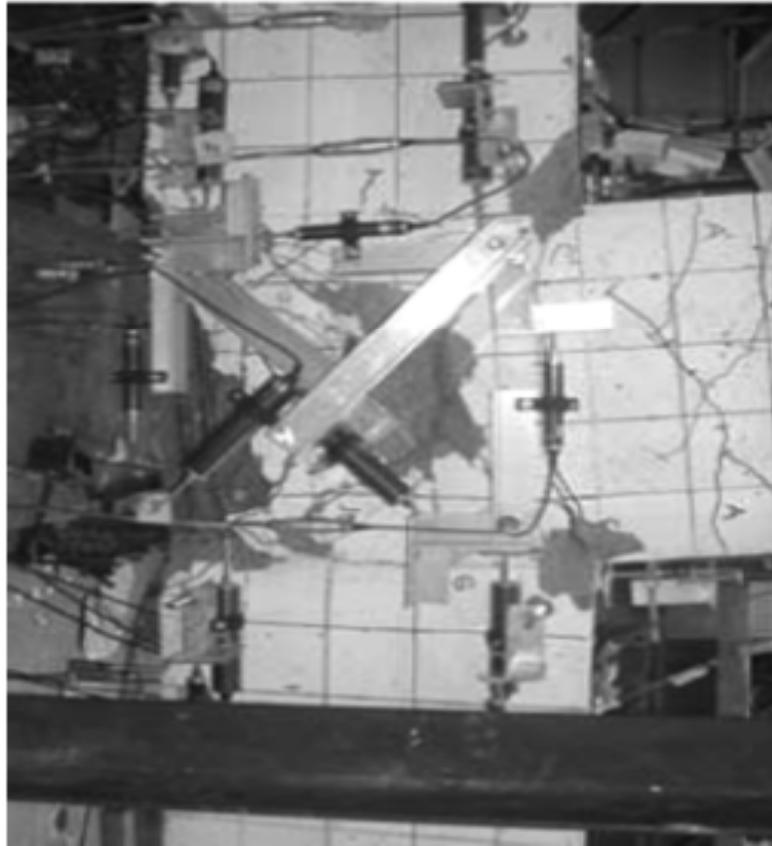
ENVELOPE FOR HYSTERESIS



LOAD VS DISPLACEMENT DIAGRAM FOR JW2



JOINT FAILURE FOR JW2



- JW2**
 A' = Closed
 B' = Closed
 C' = 5.00 mm
 D' = 3.00 mm
 E' = Closed
 F' = 0.35 mm
 G' = 3.00 mm
 H' = 1.50 mm
 JA' = 4.00 mm
 JB' = 4.00 mm
 JC' = 1.30 mm

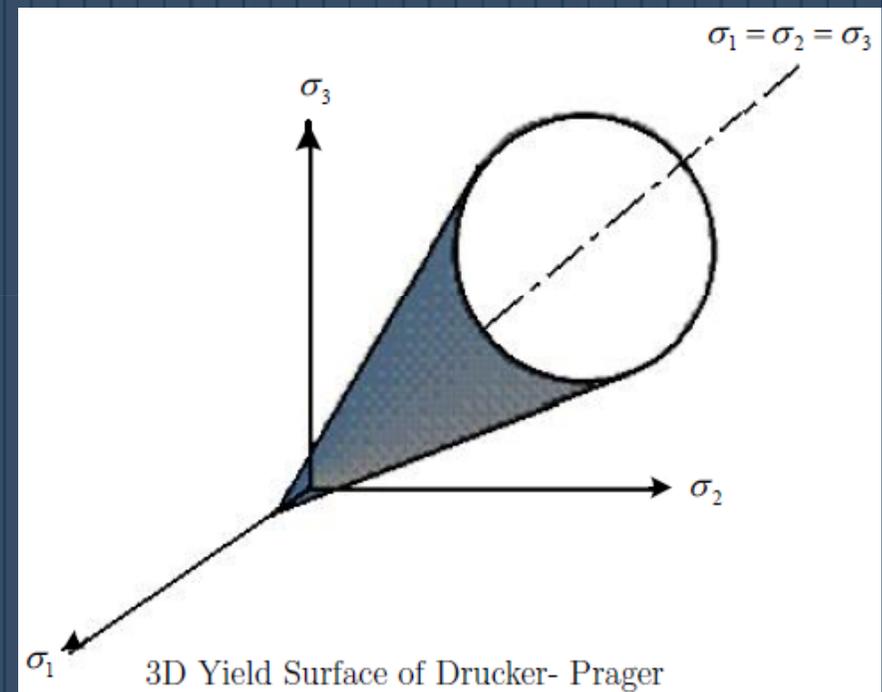
- A = Closed
 B = 0.20 mm
 C = 7.00 mm
 D = 1.40 mm
 E < 0.10 mm
 F = 0.70 mm
 G = 2.20 mm
 H = 0.40 mm
 JA = 4.00 mm
 JB = 2.00 mm
 I = 0.30 mm
 JC = 0.60 mm
 K = 0.20 mm

FINITE ELEMENT MODELING

- The commercial F.E software DIANA is used which is well known for modeling concrete structures due to its wide range of concrete material models and advanced numerical tools.
- The non-linear mechanisms that are considered in the modeling are cracking and crushing of concrete and yielding of reinforcement.
- The finite element model is two dimensional consisting of plane stress elements.

MATERIAL CONSTITUTIVE MODELS

- Concrete Plasticity :
- Concrete is modeled as elastic perfectly plastic.
- Drucker-Prager yield criterion is used to model the stress level at which yielding of concrete is initiated.
- The yield surface of Drucker-Prager model is a circular cone which can be related to Mohr-Coulomb by expressing α and k in terms of c and ϕ .
- In Drucker-Prager plasticity model, associated plasticity is established by setting $\phi = \psi$.

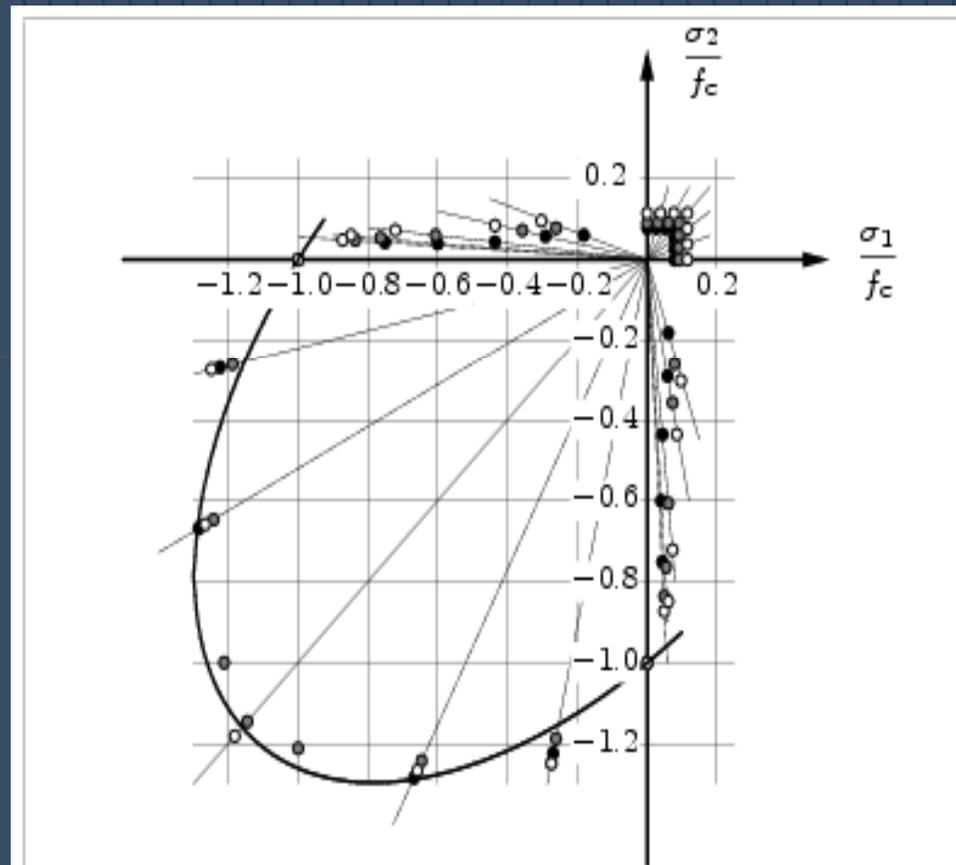


MATERIAL CONSTITUTIVE MODELS

- The cohesion is related to the concrete strength through the relation given by

$$c = f'_c \left[\frac{1 - \sin \phi}{2 \cos \phi} \right]$$

- For the normal strength quality concrete, the ratio between the biaxial compressive strength and uniaxial compressive strength is approximately 1:1.16 which results in a friction angle $\phi=10\text{deg}$ and cohesion $c=0.42f'_c$



Biaxial strength of plain concrete, Kupfer and Gerstle

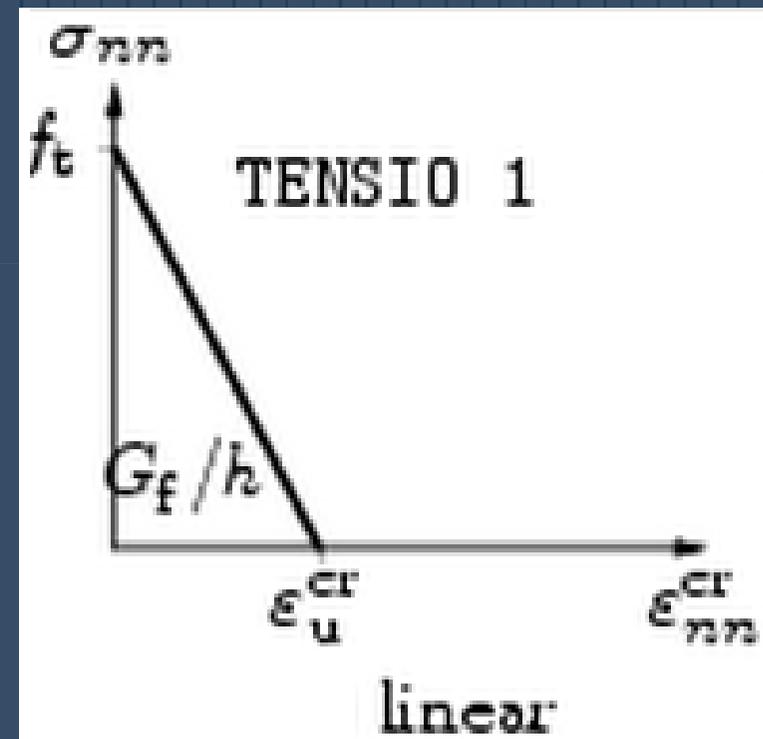
MATERIAL CONSTITUTIVE MODELS

- **Concrete cracking:**

The cracking of the concrete is specified as a combination of constant tension cut-off, linear tension softening and shear retention.

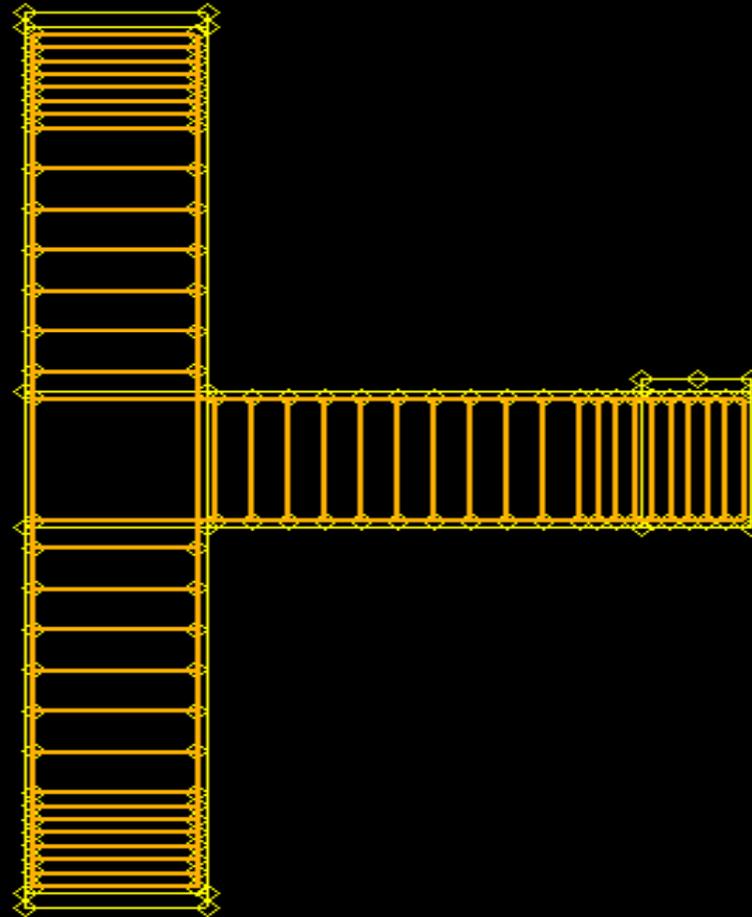
- **Reinforcement:**

For reinforcement Von-Mises-Plasticity with work hardening is used.



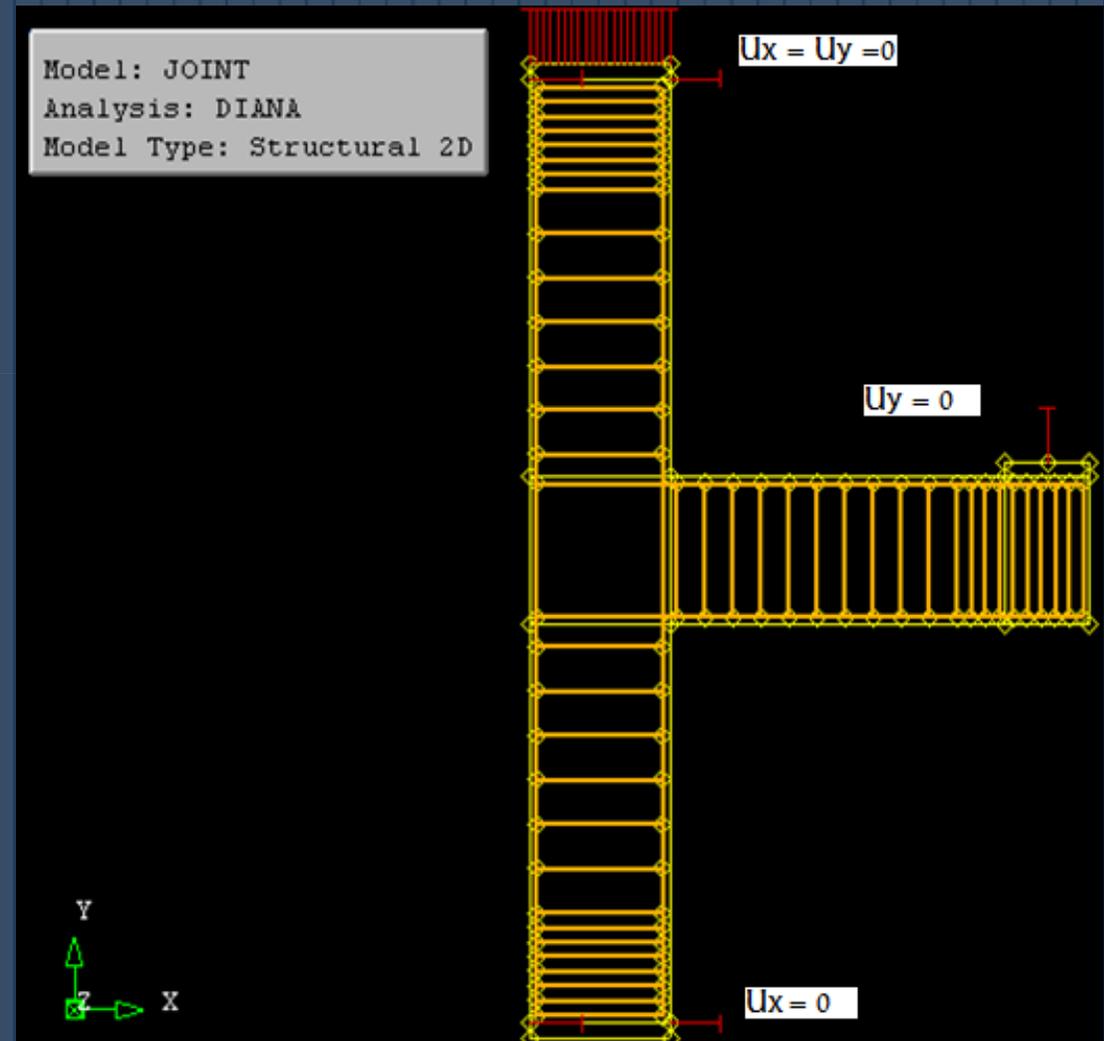
2-D MODEL WITH REINFORCEMENT

Model: JOINT
Analysis: DIANA
Model Type: Structural 2D



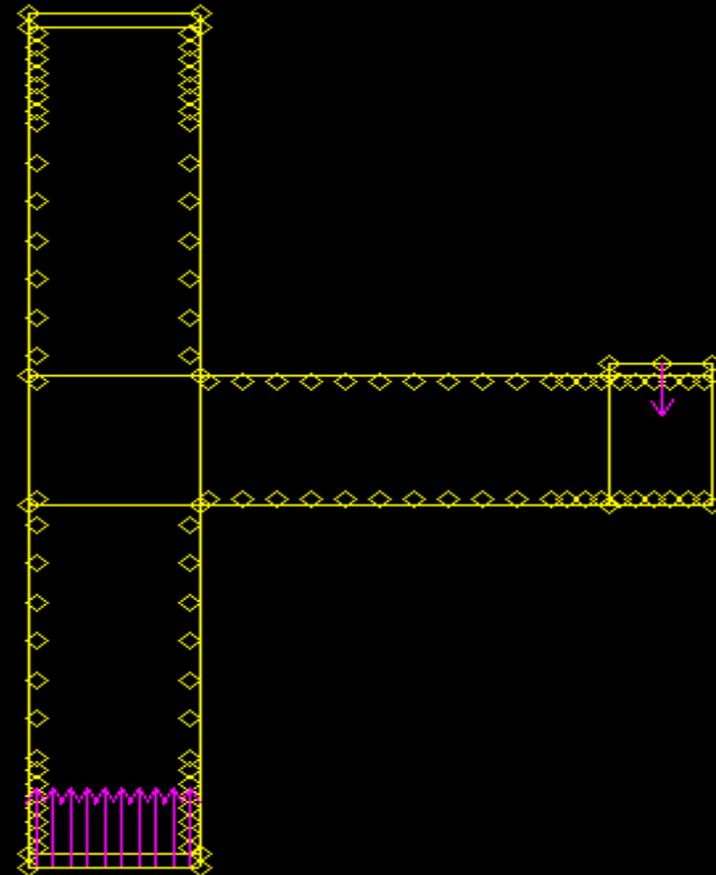
BOUNDARY CONDITIONS AND LOADING DETAILS

- Top end of the column surface is constrained in X and Y direction
- Bottom end of the column is constrained in X axis and free in Y direction due to upward axial pressure ($0.125 \cdot f'_c$).
- Near the tip of beam point is constrained in y direction because loading method is displacement control which is 50mm



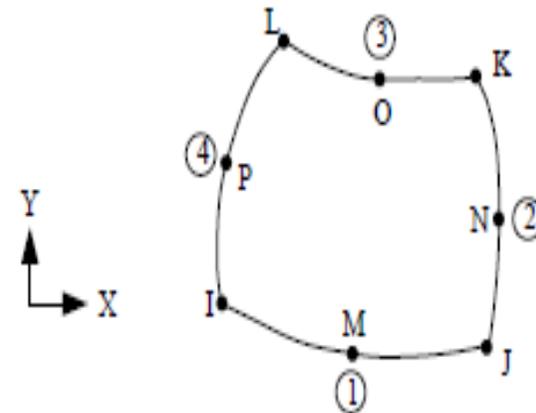
BOUNDARY CONDITIONS AND LOADING DETAILS

Model: JOINT
Analysis: DIANA
Model Type: Structural 2D



FINITE ELEMENT MESH

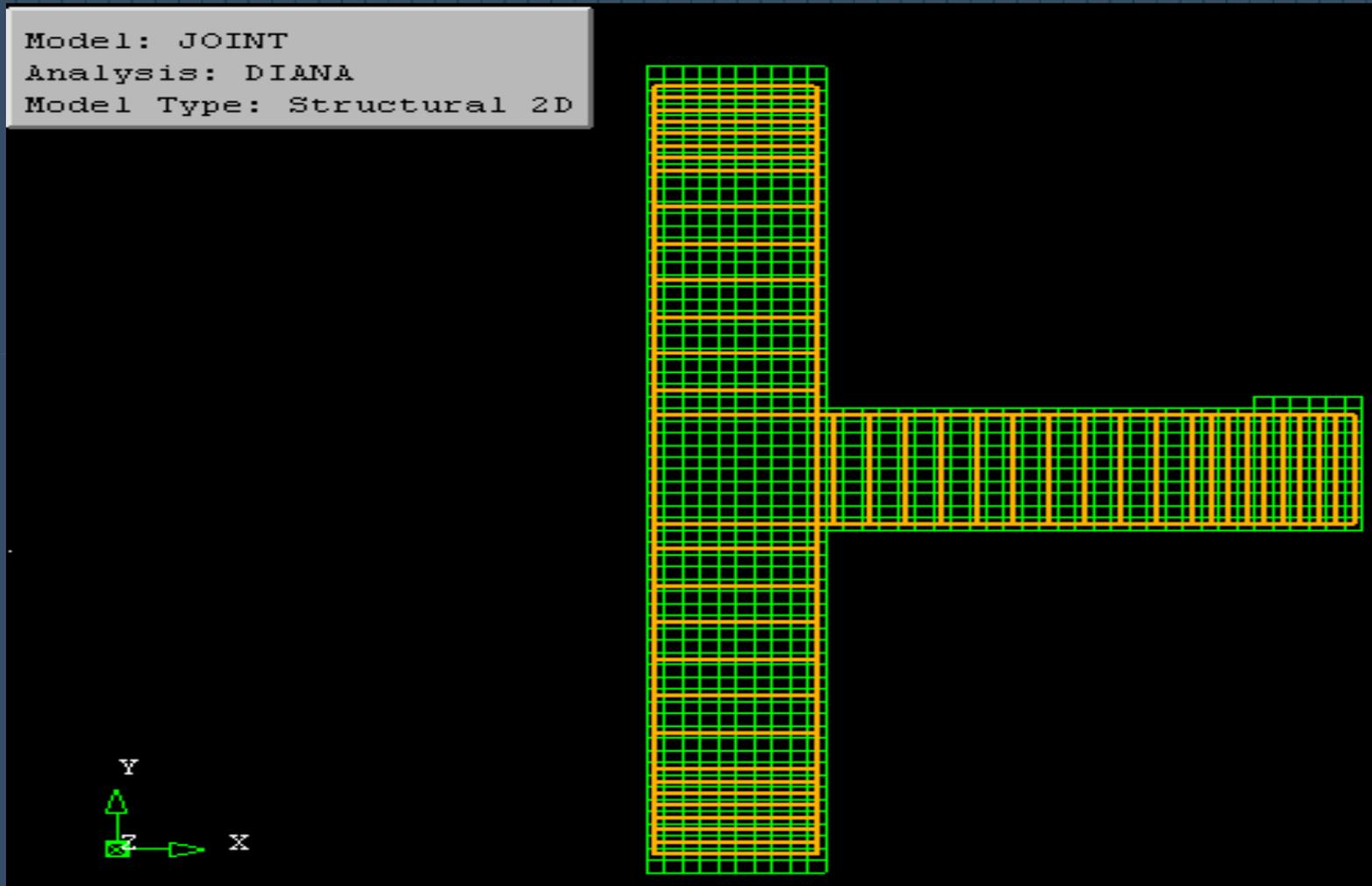
- The concrete is modeled by eight-noded quadrilateral isoparametric plane stress element CQ16M.
- The mesh size of concrete element is 50x50 (mm).
- Reinforcements are modeled as embedded reinforcement.



Eight-node Quadrilateral Isoparametric Plane Stress Elements

MESH WITH REINFORCEMENT

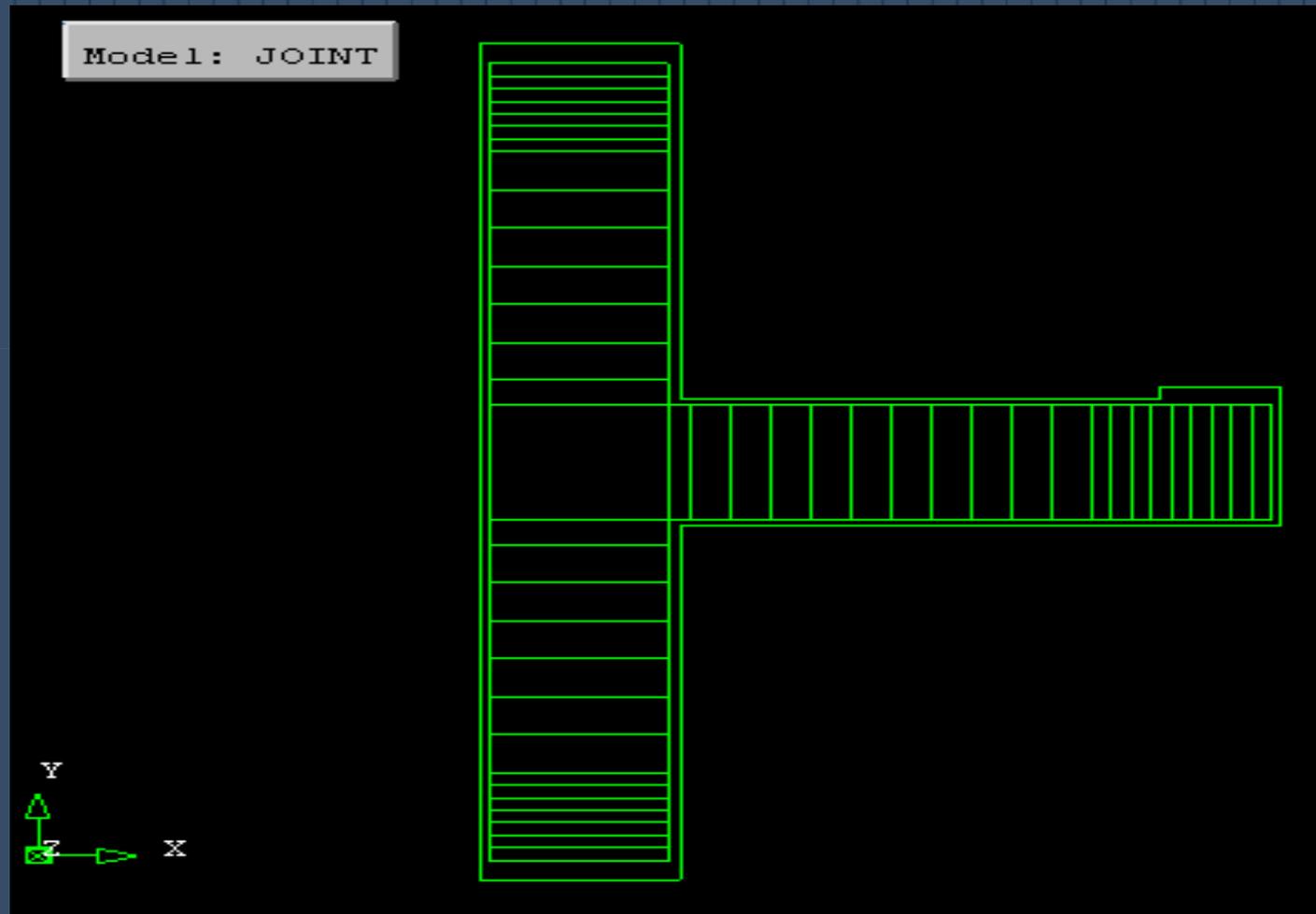
Model: JOINT
Analysis: DIANA
Model Type: Structural 2D



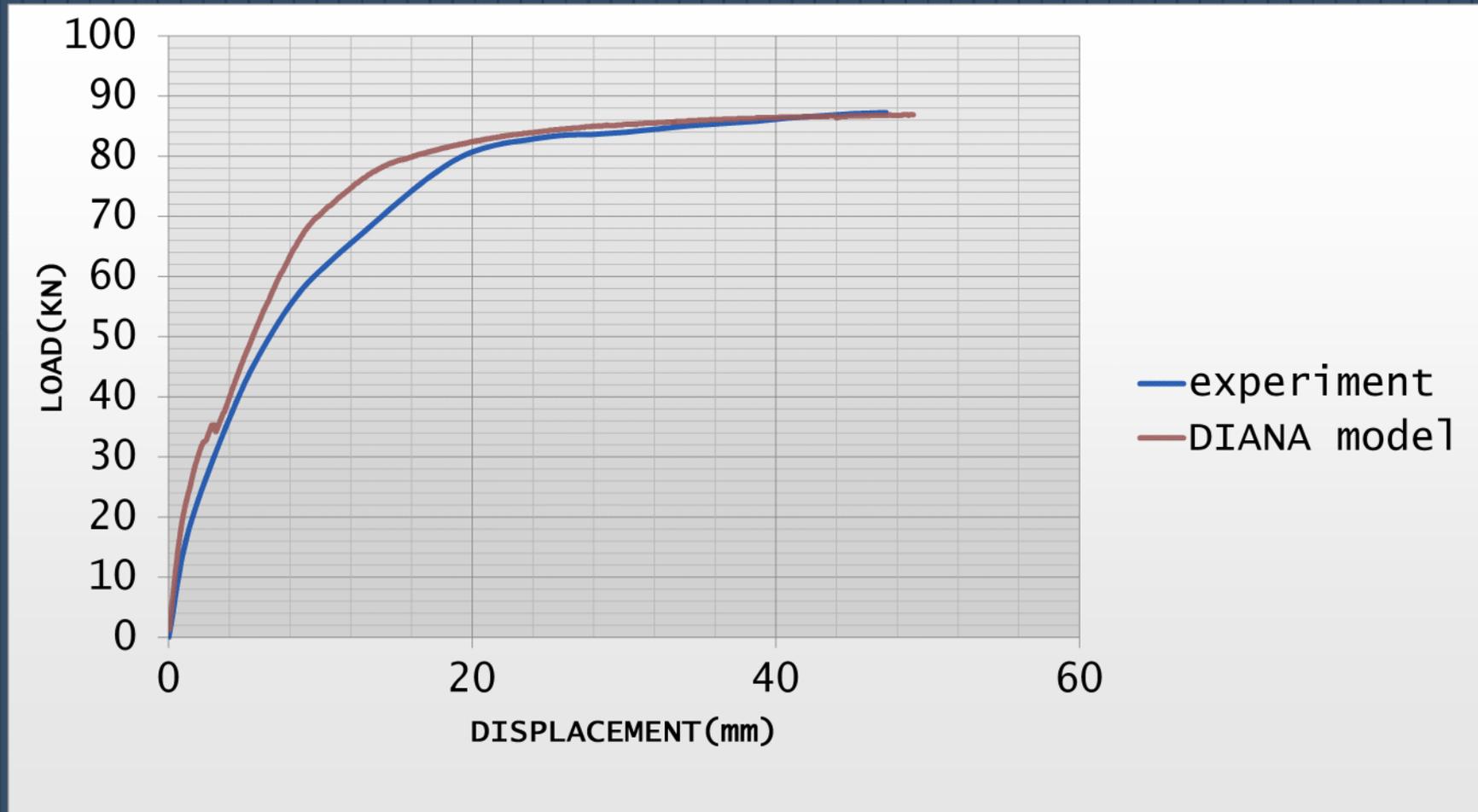
DIANA ANALYSIS

- DIANA needs two files to start the analysis
 1. (.dat) file which contains material properties for concrete $f_t=0.73\text{Mpa}$ at 28 days, $c=2.15\text{Mpa}$ (calibrated to match experimental data), $\phi = \psi=10\text{deg}$, $\beta=0.9$ (smaller values lead to premature curtailment of P- Δ curve), $E=12000\text{Mpa}$ and steel (hardening diagram and modulus of elasticity) , Nodal coordinates , Reinforcement coordinates, Boundary conditions and Load cases.
 2. (.com) file where we define the iteration method, step size (load step 0.050mm) and convergence criteria for analysis.

FINITE ELEMENT ANALYSIS RESULTS



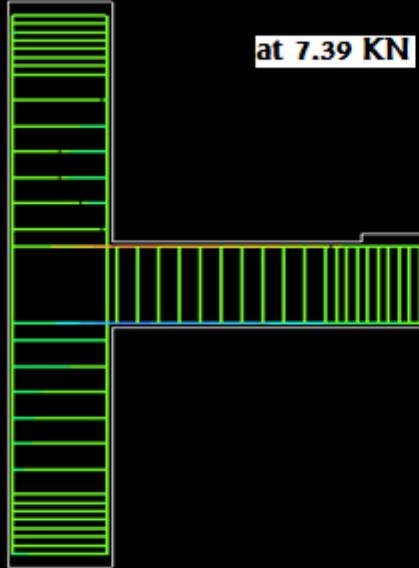
LOAD VS DISPLACEMENT DIAGRAM FOR JW2 AND DIANA MODEL



STRESS IN STEEL SXX (BEAM)

Model: JOINT
 LC2: Load case 2
 Step: 6 LOAD: .5E-2
 Element RE.SXX.G SXX
 Max = 10
 Min = -8.59

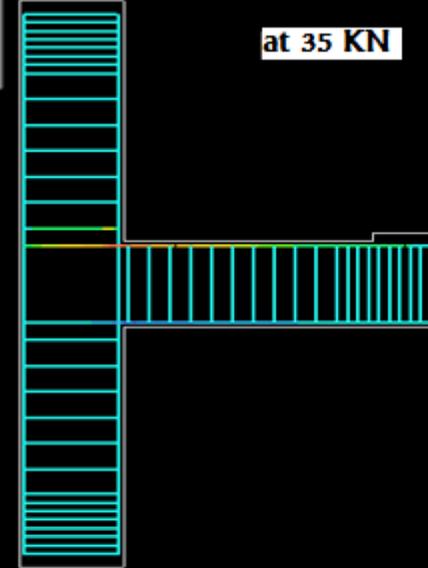
at 7.39 KN



8.32
 6.63
 4.94
 3.25
 1.56
 -.134
 -1.83
 -3.52
 -5.21
 -6.9

Model: JOINT
 LC2: Load case 2
 Step: 56 LOAD: .55E-1
 Element RE.SXX.G SXX
 Max = 146 Min = -78.7

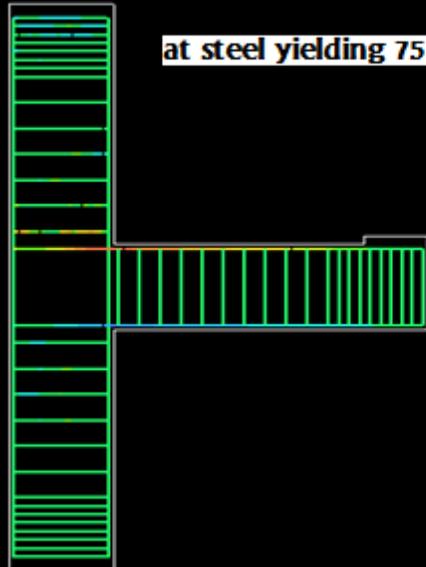
at 35 KN



125
 105
 84.6
 64.2
 43.8
 23.4
 2.93
 -17.5
 -37.9
 -58.3

Model: JOINT
 LC2: Load case 2
 Step: 243 LOAD: .242
 Element RE.SXX.G SXX
 Max = 326 Min = -194

at steel yielding 75 KN



279
 232
 184
 137
 89.7
 42.4
 -4.94
 -52.2
 -99.6
 -147

Model: JOINT
 LC2: Load case 2
 Step: 982 LOAD: .981
 Element RE.SXX.G SXX
 Max = 352 Min = -311

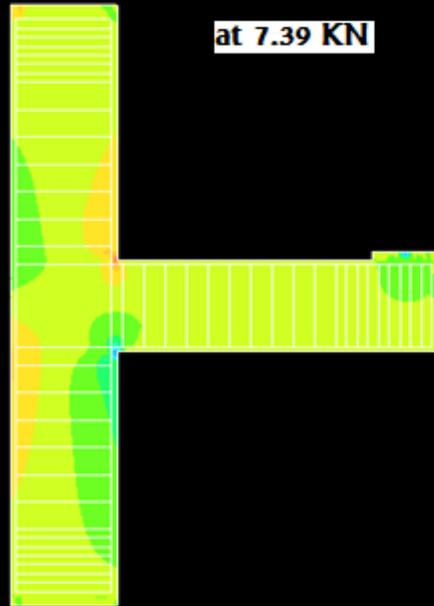
at ultimate load
 86.9 KN



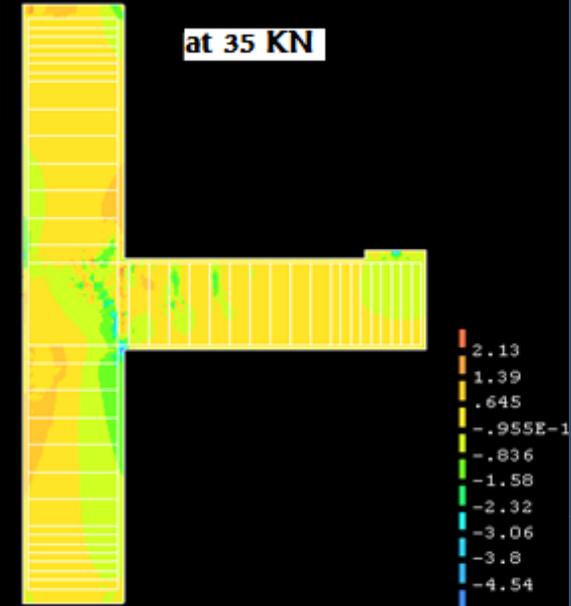
292
 232
 171
 111
 50.9
 -9.4
 -69.7
 -130
 -190
 -251

STRESSES IN CONCRETE SYY (COLUMN)

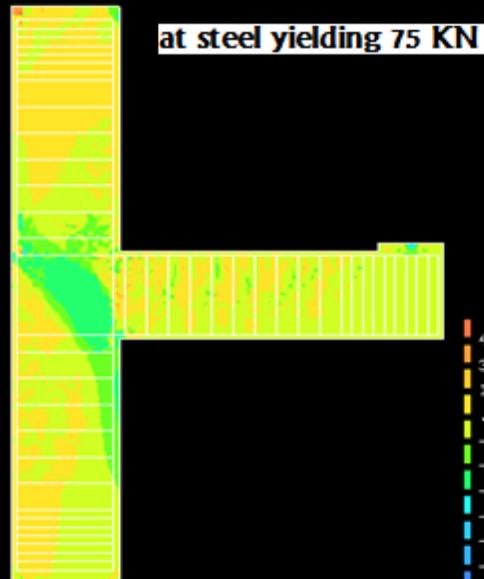
Model: JOINT
 LC2: Load case 2
 Step: 6 LOAD: .5E-2
 Element EL.SXX.G SYY
 Max = .681
 Min = -.896



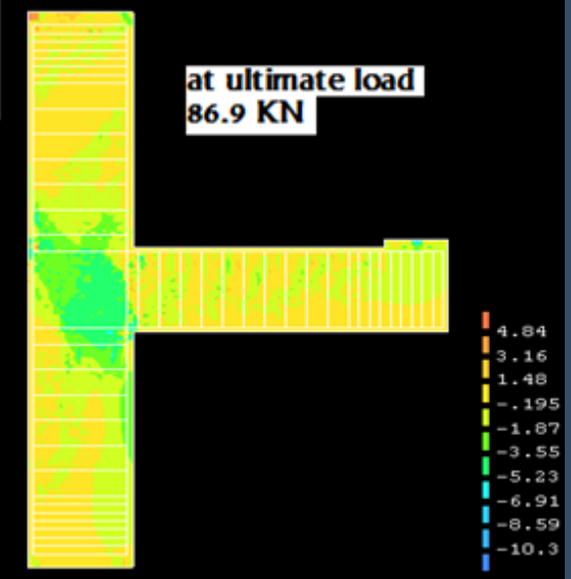
Model: JOINT
 LC2: Load case 2
 Step: 56 LOAD: .55E-1
 Element EL.SXX.G SYY
 Max = 2.87
 Min = -5.28



Model: JOINT
 LC2: Load case 2
 Step: 243 LOAD: .242
 Element EL.SXX.G SYY
 Max = 6 Min = -10.3

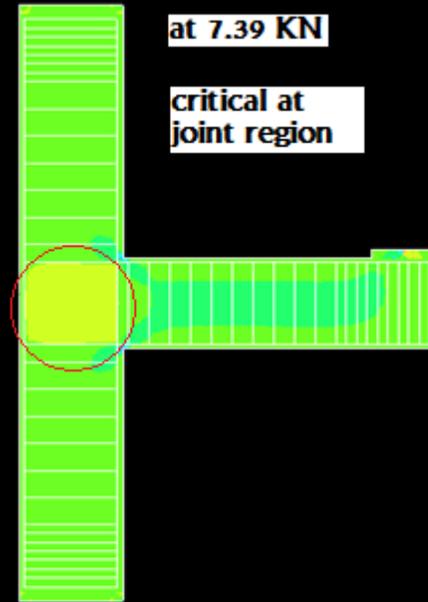


Model: JOINT
 LC2: Load case 2
 Step: 982 LOAD: .981
 Element EL.SXX.G SYY
 Max = 6.52
 Min = -11.9

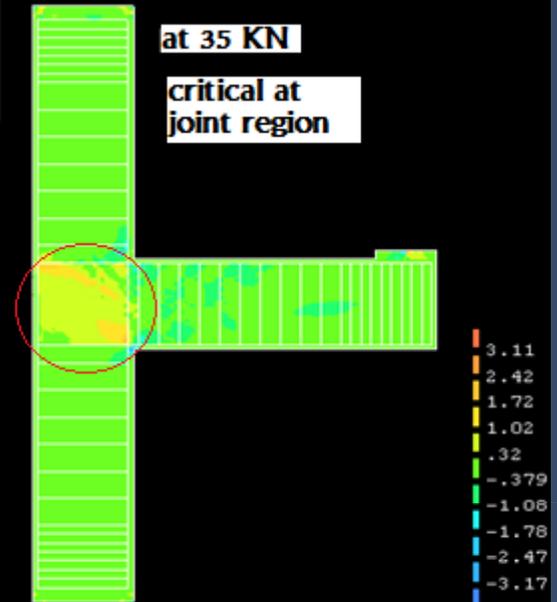


STRESSES IN CONCRETE SXY

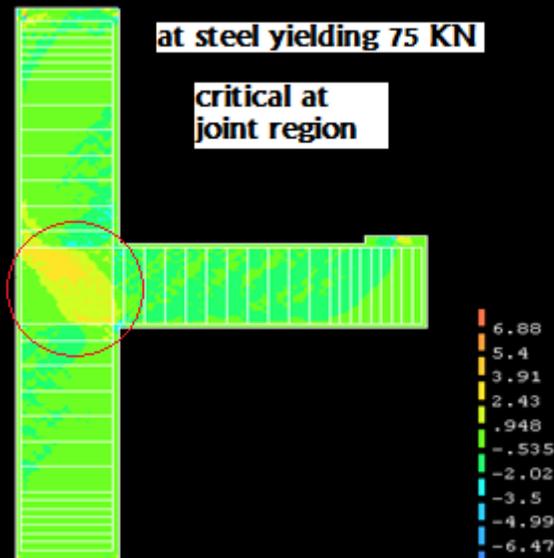
Model: JOINT
 LC2: Load case 2
 Step: 6 LOAD: .5E-2
 Element EL.SXX.G SXY
 Max = .68
 Min = -.668



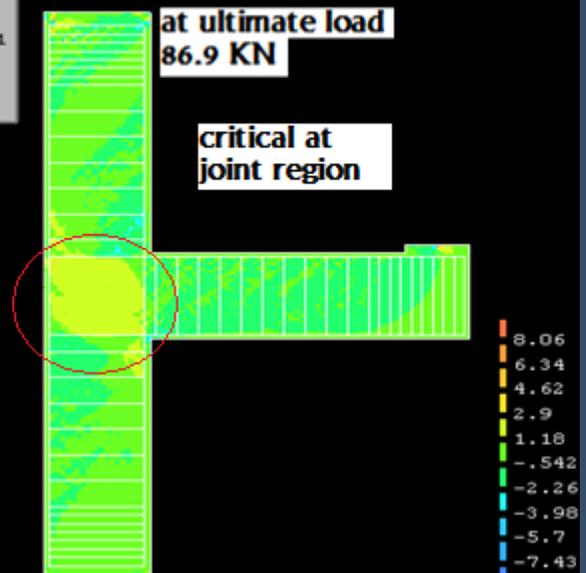
Model: JOINT
 LC2: Load case 2
 Step: 56 LOAD: .55E-1
 Element EL.SXX.G SXY
 Max = 3.81
 Min = -3.87



Model: JOINT
 LC2: Load case 2
 Step: 243 LOAD: .242
 Element EL.SXX.G SXY
 Max = 8.36
 Min = -7.95



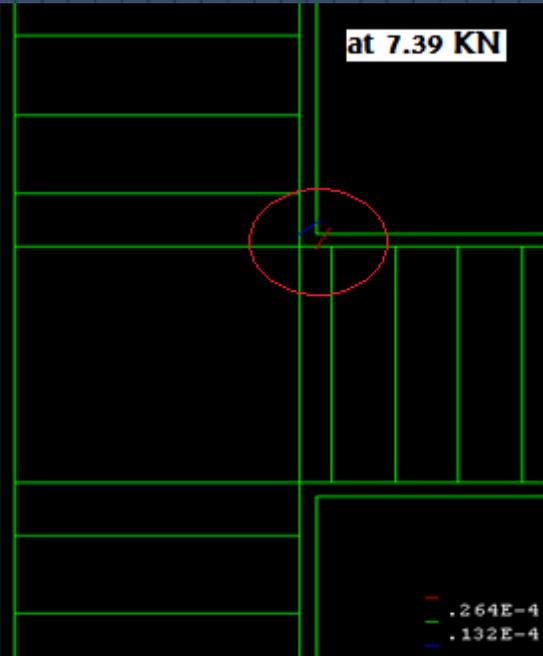
Model: JOINT
 LC2: Load case 2
 Step: 982 LOAD: .981
 Element EL.SXX.G SXY
 Max = 9.79
 Min = -9.15



CRACK PATTERNS

Model: JOINT
LC2: Load case 2
Step: 6 LOAD: .5E-2
Gauss EL.EKNN1 EKNN
Max = .396E-4
Min = 0

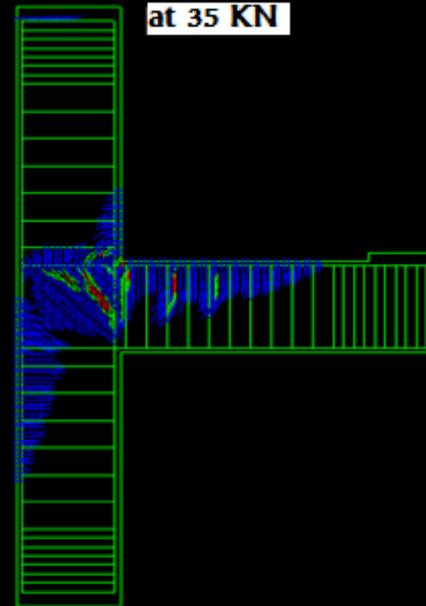
at 7.39 KN



.264E-4
.132E-4

Model: JOINT
LC2: Load case 2
Step: 56 LOAD: .55E-1
Gauss EL.EKNN1 EKNN
Max = .301E-2 Min = 0

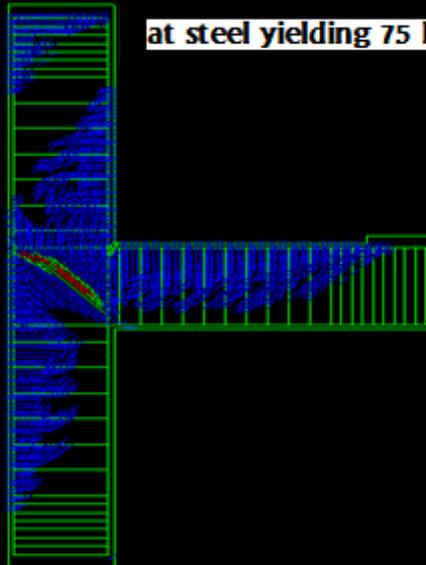
at 35 KN



.201E-2
.1E-2

Model: JOINT
LC2: Load case 2
Step: 243 LOAD: .242
Gauss EL.EKNN1 EKNN
Max = .209E-1
Min = 0

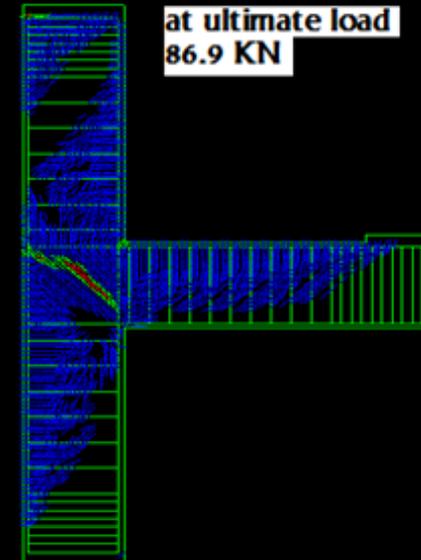
at steel yielding 75 KN



.139E-1
.696E-2

Model: JOINT
LC2: Load case 2
Step: 982 LOAD: .981
Gauss EL.EKNN1 EKNN
Max = .11 Min = 0

at ultimate load
86.9 KN



.733E-1
.366E-1

CONCLUSIONS

- The finite element simulation of the represented by the load-deflection shows good agreement with the test data which indicates that DIANA software with its 2-D plane stress model is able to capture the behavior of beam-column joint well.
- The crack patterns at various loads from the FE model correspond well with the experimentally observed failure modes, stresses in the beam, column and joints are in agreement.

WORK IN PROGRESS AT KFUPM

- In a collaborative program presently underway between Istanbul Technical university (ITU) and King Fahd University of Petroleum and Minerals (KFUPM) an experimental program is being conducted at KFUPM on the beam-column joints used in old reinforced concrete buildings in Saudi Arabia.
- Finite element simulation has been done for the static load test to capture the nonlinear behavior of the joint.

ACKNOWLEDGEMENT KFUPM

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- The authors acknowledge the mentoring provided by ITU to the KFUPM graduate students involved in this project.