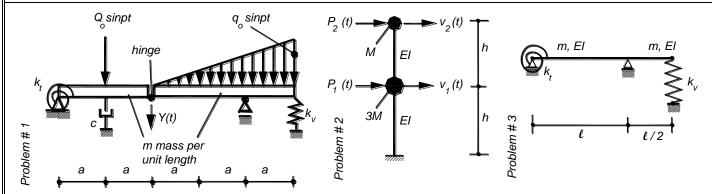
ADVANCED DYNAMICS OF STRUCTURES Final Exam January 12, 2009 / HBoduroğlu/ZCelep



Problem#1

For the rigid-body assemblage shown set up the equation of motion in terms of the vertical displacement Y(t) of the hinge by using the principle of the virtual work. By assuming $k_t = 2 k_v a^2$, determine the period of the system as $T = \alpha \sqrt{m a/k_v}$ and evaluate α .

Problem#2

- a. Write down equation of motion of the column having two-degree-of-freedom including the external forces $P_1(t)$ and $P_2(t)$.
- b. Obtain the mass matrix \mathbf{m} , the stiffness matrix \mathbf{k} and the flexibility matrix $\mathbf{d} = \mathbf{k}^{-1}$.
- c. Determine the two circular frequencies $\omega_1 < \omega_2$, the two periods of the free vibration $T_i = \alpha_i \sqrt{M \ h^3}/(EI)$ $T_1 > T_2$ including α_1 and the corresponding mode shapes ϕ_1 , and ϕ_2 . Give their graphical representations.
- d. Check the orthogonality of the modes with respect to the mass matrix $\phi_1^T \mathbf{m} \phi_2$ and the stiffness matrix $\phi_1^T \mathbf{k} \phi_2$.
- e. Evaluate the generalized masses and stiffness M_1 , M_2 and K_1 , K_2 and assess that $\omega_i^2 = K_i/M_i$.
- f. Write down the discretized version of the equations of motion as $M_i \ddot{Y}_i + K_i Y_i = \phi_1^T \mathbf{p}$
- g. Assuming that the system is under the impulsive load of P_2 ad $I = \int_0^{t_O} P_2(\tau) d\tau = P_o t_o$ and $P_1(t) = 0$ and assuming that the system starts from the rest, i.e., $v(t=0) = \dot{v}(t=0) = 0$ and $t_o << T_2 < T_1$, obtain $Y_i(t)$ and $v_i(t)$.

Problem#3

Consider the distributed parameter system shown where m is the mass per unit length and EI is the bending rigidity of the cross section. Write down the boundary conditions for the free vibration of the beam.

Ingularly of the cross section. While down the boundary conditions for the free violation of the beam.

$$\mathbf{m} \ddot{\mathbf{v}}(t) + \mathbf{k} \mathbf{v}(t) = \mathbf{p}(t) \quad \mathbf{v}(t) = \begin{bmatrix} v_1(t) & v_2(t) \end{bmatrix}^T \quad \mathbf{p}(t)^T = \begin{bmatrix} P_1(t) & P_2(t) \end{bmatrix}$$

$$(\mathbf{k} - \omega_i^2 \mathbf{m}) \phi_i = 0 \quad \omega_i = 2\pi/T_i \quad (\mathbf{I} - \omega_i^2 \mathbf{d} \mathbf{m}) \phi_i = 0 \quad |\mathbf{k} - \omega_i^2 \mathbf{m}| = 0$$

$$K_i = \phi_i^T \mathbf{k} \phi_i \quad M_i \ddot{Y}_i(t) + K_i Y_i(t) = \phi_i^T \mathbf{p}(t) \quad v(t) = \sum_{i=1}^2 Y_i(t) \phi_i$$

$$Y_i(t) = \phi_i^T \mathbf{m} \mathbf{v}/M_i \quad Y_i(t) = \frac{\sin \omega_i t}{M_i \omega_i} \left[\phi_i^T \int_0^{t_0} \mathbf{p}(\tau) d\tau \right] \quad M_i = \phi_i^T \mathbf{m} \phi_i$$

$$I_\theta = \frac{M}{12} (a^2 + b^2) \quad v_1 = \frac{Q b^3}{3 EI} + \frac{Q c b^2}{2 EI} \quad v_2 = \frac{Q (c + b)^3}{3 EI} \quad v_1 = \frac{R b^3}{3 EI}$$

$$v_2 = \frac{R b^3}{3 EI} + \frac{R c b^2}{2 EI} \quad M(x, t) = -EI \frac{\partial^2 v}{\partial x^2} \quad V(x, t) = -EI \frac{\partial^3 v}{\partial x^3} \quad a^4 = \frac{m \omega^2}{EI}$$

$$v(x, t) = \sum \phi_i(x) Y_i(t) \quad \phi(x) = A_1 \sin ax + A_2 \cos ax + A_3 \sinh ax + A_4 \cosh ax \quad \ddot{Y}_i(t) + \omega_i^2 Y_i(t) = 0$$