

PROJECT # 3

The Euler equations governing unsteady compressible inviscid flows can be expressed in conservative form as:

$$\frac{\partial Q}{\partial t} + \frac{\partial F_1}{\partial x_1} + \frac{\partial F_2}{\partial x_2} = 0 \quad (1)$$

where

$$Q = \begin{bmatrix} \rho \\ \rho u_1 \\ \rho u_2 \\ E \end{bmatrix} \quad F_1 = \begin{bmatrix} \rho u_1 \\ \rho u_1^2 + p \\ \rho u_1 u_2 \\ u_1(E + p) \end{bmatrix} \quad F_2 = \begin{bmatrix} \rho u_2 \\ \rho u_1 u_2 \\ \rho u_2^2 + p \\ u_2(E + p) \end{bmatrix} \quad (2)$$

and the internal energy of the gas

$$E = \rho e_{int} + \frac{1}{2} \rho (u_1^2 + u_2^2) \quad (3)$$

The Euler equations are not complete without an equation of state. We choose an ideal gas for which

$$e_{int} = \frac{p}{\rho(\gamma - 1)} \quad (4)$$

The initial conditions are $\rho = 1.4$, $u = 3$, $v = 0$ and $p = 1$. Use the Euler explicit and the fourth-order Runge-Kutta (optional) method with AUSM⁺-up scheme [1], to solve the forward facing step problem given in Figure 1 at $t = 4$. The state variables Q are defined at the cell centers. The unstructured

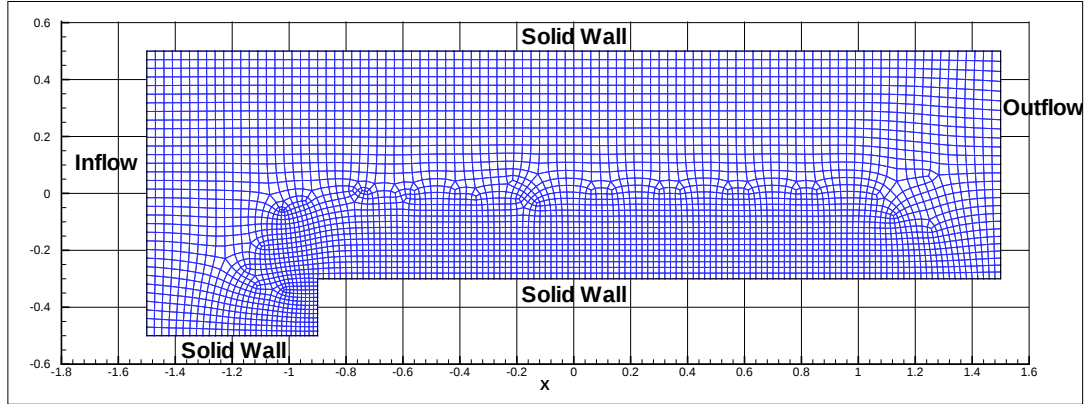


Figure 1: The forward step problem at $M_\infty = 3$ with boundary conditions.

mesh data is available at: http://web.itu.edu.tr/~msahin/utt619e_2011/forward_step.neu and the neighbouring element numbers are given at: http://web.itu.edu.tr/~msahin/utt619e_2011/fort.60. The zero value indicates that there is no neighbour for that element edge since it is next to the boundary.

The AUSM⁺-up Flux

The AUSM⁺-up for all speeds

$$M_{L/R} = \frac{\mathbf{n} \cdot \mathbf{u}_{L/R}}{a_{1/2}} \quad (5)$$

where $a_{1/2} = (a_L + a_R)/2$

$$\bar{M}^2 = \frac{|\mathbf{u}_L|^2 + |\mathbf{u}_R|^2}{2a_{1/2}^2} \quad (6)$$

$$M_0^2 = \min(1, \max(\bar{M}^2, M_\infty^2)) \quad (7)$$

$$f_a(M_0) = M_0(2 - M_0) \quad (8)$$

$$\rho_{1/2} = \frac{\rho_L + \rho_R}{2} \quad (9)$$

$$M_{1/2} = M_{(4)}^+(M_L) + M_{(4)}^-(M_R) - \frac{K_p}{f_a} \max(1 - \sigma \bar{M}^2, 0) \frac{p_R - p_L}{\rho_{1/2} a_{1/2}^2} \quad (10)$$

where

$$M_{(4)}^\pm(M) = \begin{cases} \frac{1}{2}(M \pm |M|) & \text{if } |M| \geq 1 \\ \pm \frac{1}{4}(M \pm 1)^2(1 + 16\beta \frac{1}{4}(M \mp 1)^2) & \text{otherwise} \end{cases} \quad (11)$$

and $\rho_{1/2} = (\rho_L + \rho_R)/2$, $K_p = 0.25$ and $\sigma = 1$. Then the mass flux

$$\dot{m}_{1/2} = \begin{cases} a_{1/2} M_{1/2} \rho_L & \text{if } M_{1/2} > 0 \\ a_{1/2} M_{1/2} \rho_R & \text{otherwise} \end{cases} \quad (12)$$

the pressure flux

$$p_{1/2} = P_{(5)}^+(M_L)p_L + P_{(5)}^-(M_R)p_R - K_u P_{(5)}^+(M_L)P_{(5)}^-(M_R)(\rho_L + \rho_R)(f_a a_{1/2}^2)(M_R - M_L) \quad (13)$$

and

$$P_{(5)}^\pm(M) = \begin{cases} \frac{1}{2\bar{M}}(M \pm |M|) & \text{if } |M| \geq 1 \\ \pm \frac{1}{4}(M \pm 1)^2 [(\pm 2 - M) + 16\alpha M \frac{1}{4}(M \mp 1)^2] & \text{otherwise} \end{cases} \quad (14)$$

using the parameters

$$\alpha = \frac{3}{16}(-4 + 5f_a^2) \quad \beta = \frac{1}{8} \quad K_u = 0.75 \quad (15)$$

The whole flux

$$\mathbf{n} \cdot \mathbf{F} = \dot{m}_{1/2} \begin{bmatrix} 1 \\ u_1 \\ u_2 \\ H \end{bmatrix} \begin{matrix} L \\ R \end{matrix} \text{ if } M_{1/2} > 0 \text{ otherwise} + \begin{bmatrix} 0 \\ p_{1/2} n_1 \\ p_{1/2} n_2 \\ 0 \end{bmatrix} \quad (16)$$

where the local enthalpy is given by

$$H = \frac{E + p}{\rho} \quad (17)$$

References

- [1] Meng-Sing Liou, A sequel to AUSM, Part II: AUSM⁺-up for all speeds. *J. Comput. Phys.* **214**, (2006), 137–170.

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Read Mesh Vetices
for  $i \leftarrow 1$  to  $np$  do
  | read  $x[i], y[i], z[i]$ 
end

Read Element Connectivity
for  $i \leftarrow 1$  to  $ne$  do
  | read  $nec[i,1], nec[i,2], nec[i,3], nec[i,4]$ 
end

Read Neighbouring Element Numbers
for  $i \leftarrow 1$  to  $ne$  do
  | read  $fec[i,1], fec[i,2], fec[i,3], fec[i,4]$ 
end

Initial Q Value
 $Q^1 := Q_\infty$ 

Time integration
for  $Time \leftarrow 0$  to 4 do
  |
  | Compute  $Q^{n+1}$ 
  | for  $i \leftarrow 1$  to  $ne$  do
  |    $RHS := 0$ 
  |   for  $n \leftarrow 1$  to 4 do
  |     ....
  |     ....
  |     ....
  |     if Solid Wall Boundary Condition then
  |       |  $RHS := RHS + \dots$ 
  |     else if Inflow Boundary Condition then
  |       |  $RHS := RHS + \dots$ 
  |     else if Outflow Boundary Condition then
  |       |  $RHS := RHS + \dots$ 
  |     else
  |       |  $Q_L = \dots$ 
  |       |  $Q_R = \dots$ 
  |       |  $n_x = \dots$ 
  |       |  $n_y = \dots$ 
  |       | call AUSM_Flux( $Q_L, Q_R, n_x, n_y, \mathbf{n} \cdot \mathbf{F}$ )
  |       |  $RHS := RHS + \mathbf{n} \cdot \mathbf{F} \dots$ 
  |     end
  |      $\Delta Q :=$ 
  |   end
  |    $Q^{n+1} := Q^n + \Delta Q$ 
  | end
end

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Table 1: The structure of an unstructured FVM code.